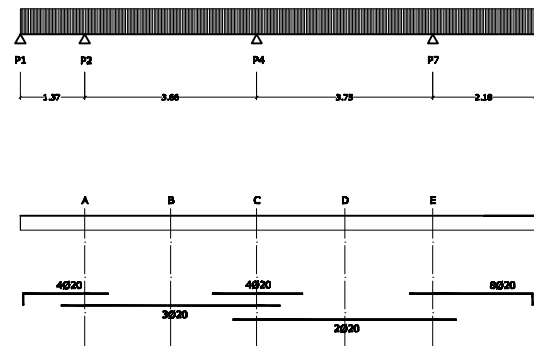
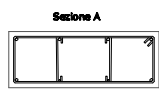


STUDIO DELLA TRAVE



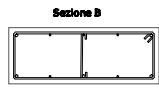
STATO LIMITE ESERCIZIO

$N_d = 1004.14 \text{ kgm}$
 $A_f \text{ min} = 0.3 \text{ N} \times 1200 / (0.90 \times 230 \times (400 \times 0.8)) = 803.80 \text{ cm}^2$
 $A_f = 8.94 \text{ cm}^2 = 3 \text{ \# } 30$
 $x = (m \times A_f / b) \times (-1 + \sqrt{1 + (2 \times b \times h) / (m \times A_f)}) = 6.87 \text{ cm}$
 $\sigma_f = N_d / (A_f \times (h - x / 3)) = 104.38 \text{ kg/cm}^2 < 20000$
 $\sigma_c = 200 / (b \times h \times (h - x / 3)) = 138.79 \text{ kg/cm}^2 < 500$

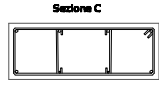


STATO LIMITE ULTIMO

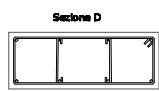
$N_d = 1533 \text{ kgm}$
 $A_f \text{ min} = 0.207 \times 1200 / (0.90 \times 230 \times (400 \times 0.8)) = 1023.32 \text{ cm}^2$
 $A_f = 10.23 \text{ cm}^2 = 4 \text{ \# } 30$
 $x = (m \times A_f / b) \times (-1 + \sqrt{1 + (2 \times b \times h) / (m \times A_f)}) = 8.26 \text{ cm}$
 $\sigma_f = 0.8 \text{ N} \times \text{Ed} \times \text{Ipo} = 22750.03 \text{ kgm}$
 $\sigma_c = 7.6 \times A_f = 76950.52 \text{ kgm}$
 $N_d = R_c \times x = (0.8 \times \text{Ed} \times \text{Ipo}) \times x = 17748.9 \text{ kgm} \Rightarrow 21.87$
 Nido-Med



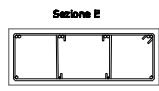
$N_d = 1388 \text{ kgm}$
 $A_f \text{ min} = 0.207 \times 1200 / (0.90 \times 230 \times (400 \times 0.8)) = 962.88 \text{ cm}^2$
 $A_f = 8.42 \text{ cm}^2 = 3 \text{ \# } 30$
 $x = (m \times A_f / b) \times (-1 + \sqrt{1 + (2 \times b \times h) / (m \times A_f)}) = 7.87 \text{ cm}$
 $\sigma_f = 0.8 \text{ N} \times \text{Ed} \times \text{Ipo} = 21365.03 \text{ kgm}$
 $\sigma_c = 7.6 \times A_f = 63582.07 \text{ kgm}$
 $N_d = R_c \times x = (0.8 \times \text{Ed} \times \text{Ipo}) \times x = 18088.87 \text{ kgm} \Rightarrow 21.87$
 Nido-Med



$N_d = 1472 \text{ kgm}$
 $A_f \text{ min} = 0.207 \times 1200 / (0.90 \times 230 \times (400 \times 0.8)) = 987.88 \text{ cm}^2$
 $A_f = 8.88 \text{ cm}^2 = 4 \text{ \# } 30$
 $x = (m \times A_f / b) \times (-1 + \sqrt{1 + (2 \times b \times h) / (m \times A_f)}) = 8.1 \text{ cm}$
 $\sigma_f = 0.8 \text{ N} \times \text{Ed} \times \text{Ipo} = 24600.03 \text{ kgm}$
 $\sigma_c = 7.6 \times A_f = 66825.48 \text{ kgm}$
 $N_d = R_c \times x = (0.8 \times \text{Ed} \times \text{Ipo}) \times x = 17764.9 \text{ kgm} \Rightarrow 21.87$
 Nido-Med



$N_d = 738.2 \text{ kgm}$
 $A_f \text{ min} = 0.207 \times 1200 / (0.90 \times 230 \times (400 \times 0.8)) = 488.94 \text{ cm}^2$
 $A_f = 4.89 \text{ cm}^2 = 2 \text{ \# } 30$
 $x = (m \times A_f / b) \times (-1 + \sqrt{1 + (2 \times b \times h) / (m \times A_f)}) = 8.89 \text{ cm}$
 $\sigma_f = 0.8 \text{ N} \times \text{Ed} \times \text{Ipo} = 4680.03 \text{ kgm}$
 $\sigma_c = 7.6 \times A_f = 18025.89 \text{ kgm}$
 $N_d = R_c \times x = (0.8 \times \text{Ed} \times \text{Ipo}) \times x = 18088.89 \text{ kgm} \Rightarrow 21.87$
 Nido-Med



$N_d = 2688 \text{ kgm}$
 $A_f \text{ min} = 0.207 \times 1200 / (0.90 \times 230 \times (400 \times 0.8)) = 2445.48 \text{ cm}^2$
 $A_f = 24.18 \text{ cm}^2 = 8 \text{ \# } 30$
 $x = (m \times A_f / b) \times (-1 + \sqrt{1 + (2 \times b \times h) / (m \times A_f)}) = 11.89 \text{ cm}$
 $\sigma_f = 0.8 \text{ N} \times \text{Ed} \times \text{Ipo} = 78283.17 \text{ kgm}$
 $\sigma_c = 7.6 \times A_f = 94258.89 \text{ kgm}$
 $N_d = R_c \times x = (0.8 \times \text{Ed} \times \text{Ipo}) \times x = 14488.38 \text{ kgm} \Rightarrow 21.87$
 Nido-Med

STATO LIMITE ESERCIZIO

Diagramma di taglio

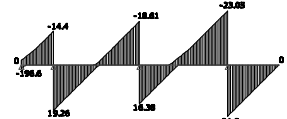
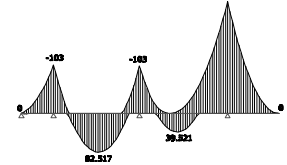


Diagramma di momenti



STATO LIMITE ULTIMO

Diagramma di taglio

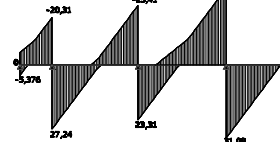
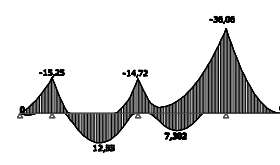
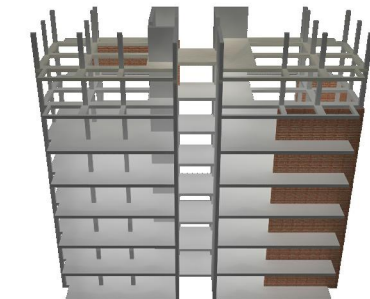
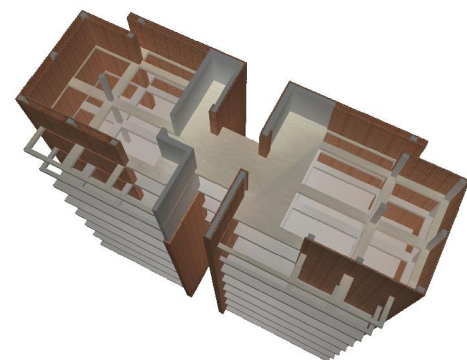
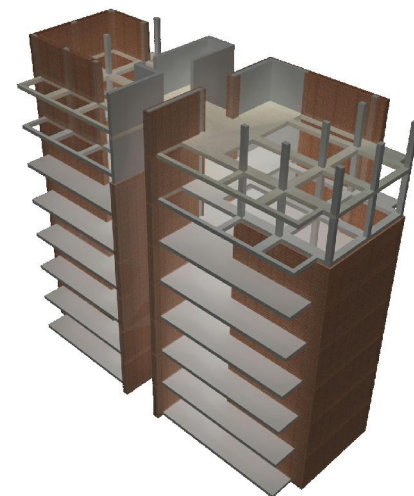
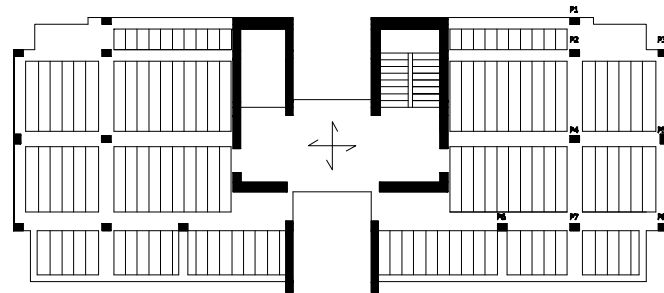


Diagramma di momenti



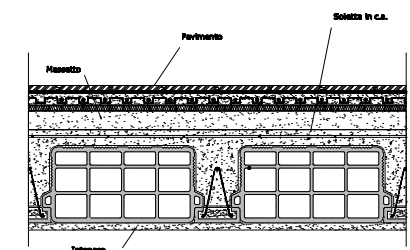
PIANTA STRUTTURALE



ANALISI DEI CARICHI-SOLAIO TIPO

Carichi accidentali Q	
Residenza	2.00 kN/m ²
Coperture	1.50 kN/m ²
Carichi Permanenti G	
Pavimento	0.81 kN/m ²
Sottotetto	0.42 kN/m ²
Tramezzi	1.30 kN/m ²
Intonaco	0.18 kN/m ²
Solaio	5.00 kN/m ²
TOTALE	7.91 kN/m²

DETTAGLIO SOLAIO



STUDIO DEL PILASTRO



$A = ((3.66 + 3.75) / 2) \times ((5.53 + 3.79) / 2) = 17.27 \text{ m}^2$
 $P, T: 10 \times 17.27 = 172.7 \text{ kN}$
 $P, C: 9.5 \times 17.27 = 164.05 \text{ kN}$
 $N_d = 172.7 \times (2 \times 164.05) = 569.45 \text{ kN}$
 $A_c \text{ min} = N_d / 0.45 \text{ Ed} = (569.45 \text{ kN} / 0.45 \times 16.6) = 681.99 \text{ cm}^2$
 Sezione Pilastro = 48 x 38
 $A_s = 0.005 \times (40 \times 25) = 4.99 \text{ cm}^2$
4812
 $A_s = 8 \# \text{ c} / 14 \text{ cm}$



$A = ((3.66 + 3.75) / 2) \times ((5.53 + 3.79) / 2) = 17.27 \text{ m}^2$
 $P, T: 10 \times 17.27 = 172.7 \text{ kN}$
 $P, C: 9.5 \times 17.27 = 164.05 \text{ kN}$
 $N_d = 172.7 \times (2 \times 164.05) = 682.15 \text{ kN}$
 $A_c \text{ min} = N_d / 0.45 \text{ Ed} = (682.15 \text{ kN} / 0.45 \times 16.6) = 913.19 \text{ cm}^2$
 Sezione Pilastro = 48 x 38
 $A_s = 0.005 \times (40 \times 25) = 5.48 \text{ cm}^2$
4816
 $A_s = 8 \# \text{ c} / 19 \text{ cm}$



$A = ((3.66 + 3.75) / 2) \times ((5.53 + 3.79) / 2) = 17.27 \text{ m}^2$
 $P, T: 10 \times 17.27 = 172.7 \text{ kN}$
 $P, C: 9.5 \times 17.27 = 164.05 \text{ kN}$
 $N_d = 172.7 \times (4 \times 164.05) = 854.85 \text{ kN}$
 $A_c \text{ min} = N_d / 0.45 \text{ Ed} = (854.85 \text{ kN} / 0.45 \times 16.6) = 1144.38 \text{ cm}^2$
 Sezione Pilastro = 48 x 38
 $A_s = 0.005 \times (40 \times 30) = 6.87 \text{ cm}^2$
4816
 $A_s = 8 \# \text{ c} / 19 \text{ cm}$



$A = ((3.66 + 3.75) / 2) \times ((5.53 + 3.79) / 2) = 17.27 \text{ m}^2$
 $P, T: 10 \times 17.27 = 172.7 \text{ kN}$
 $P, C: 9.5 \times 17.27 = 164.05 \text{ kN}$
 $N_d = 172.7 \times (8 \times 164.05) = 1027.85 \text{ kN}$
 $A_c \text{ min} = N_d / 0.45 \text{ Ed} = (1027.85 \text{ kN} / 0.45 \times 16.6) = 1375.57 \text{ cm}^2$
 Sezione Pilastro = 48 x 38
 $A_s = 0.005 \times (40 \times 25) = 8.25 \text{ cm}^2$
4816
 $A_s = 8 \# \text{ c} / 19 \text{ cm}$



$A = ((3.66 + 3.75) / 2) \times ((5.53 + 3.79) / 2) = 17.27 \text{ m}^2$
 $P, T: 10 \times 17.27 = 172.7 \text{ kN}$
 $P, C: 9.5 \times 17.27 = 164.05 \text{ kN}$
 $N_d = 172.7 \times (6 \times 164.05) = 1200.25 \text{ kN}$
 $A_c \text{ min} = N_d / 0.45 \text{ Ed} = (1200.25 \text{ kN} / 0.45 \times 16.6) = 1606.76 \text{ cm}^2$
 Sezione Pilastro = 48 x 48
 $A_s = 0.005 \times (40 \times 40) = 9.64 \text{ cm}^2$
4816
 $A_s = 8 \# \text{ c} / 19 \text{ cm}$



$A = ((3.66 + 3.75) / 2) \times ((5.53 + 3.79) / 2) = 17.27 \text{ m}^2$
 $P, T: 10 \times 17.27 = 172.7 \text{ kN}$
 $P, C: 9.5 \times 17.27 = 164.05 \text{ kN}$
 $N_d = 172.7 \times (7 \times 164.05) = 1372.97 \text{ kN}$
 $A_c \text{ min} = N_d / 0.45 \text{ Ed} = (1372.97 \text{ kN} / 0.45 \times 16.6) = 1837.97 \text{ cm}^2$
 Sezione Pilastro = 48 x 48
 $A_s = 0.005 \times (40 \times 45) = 11.02 \text{ cm}^2$
4816
 $A_s = 8 \# \text{ c} / 19 \text{ cm}$

