

## Design of primary beams

Dead load (g):  
 - g<sub>1k</sub> = ribbed slab self-weight + secondary beam self-weight + primary beams self-weight  
 = 2.65 + 0.20 + 1.52  
 = 4.37 kN/m<sup>2</sup>  
 - g<sub>2k</sub> = not structural dead loads  
 = 4.31 kN/m<sup>2</sup>

Live load (qk):  
 - occupancy load = 3 kN/m<sup>2</sup>

Snow load (qs):  
 - qs = 0.4 kN/m<sup>2</sup>

Spans of primary beams:  
 - l = 10 m

6.0- PREDIMENSIONING  
 $q = g_{1k} + g_{2k} + q_s + q_k$   
 = 4.37 + 4.31 + 3  
 = 11.68 kN

$I_{min} = 200 * 5 / 384 * q l^3 / E$   
 = 200 \* 5 / 384 \* 11.68 \* (10)<sup>3</sup> / 210000  
 = 14460 kN/m

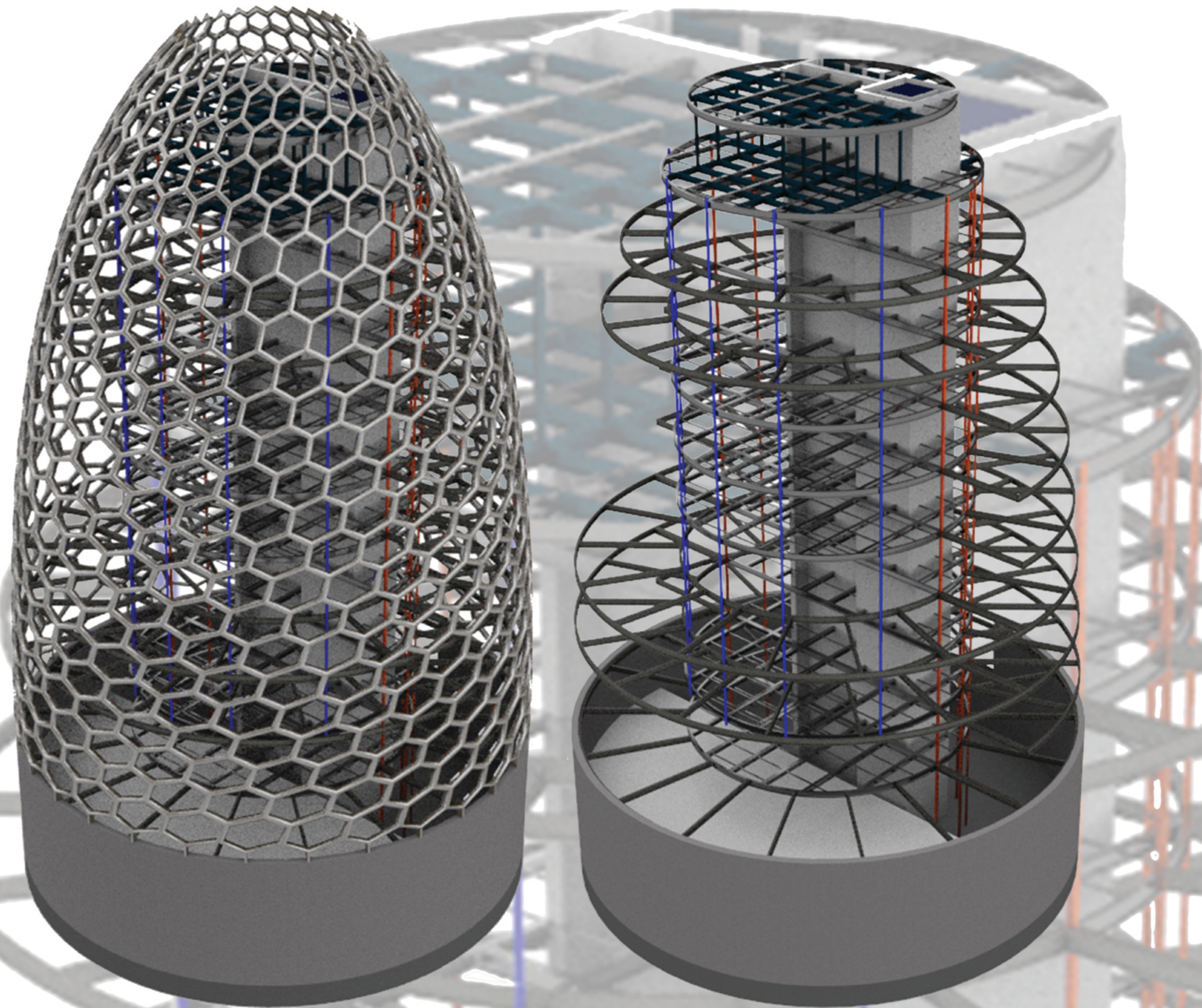
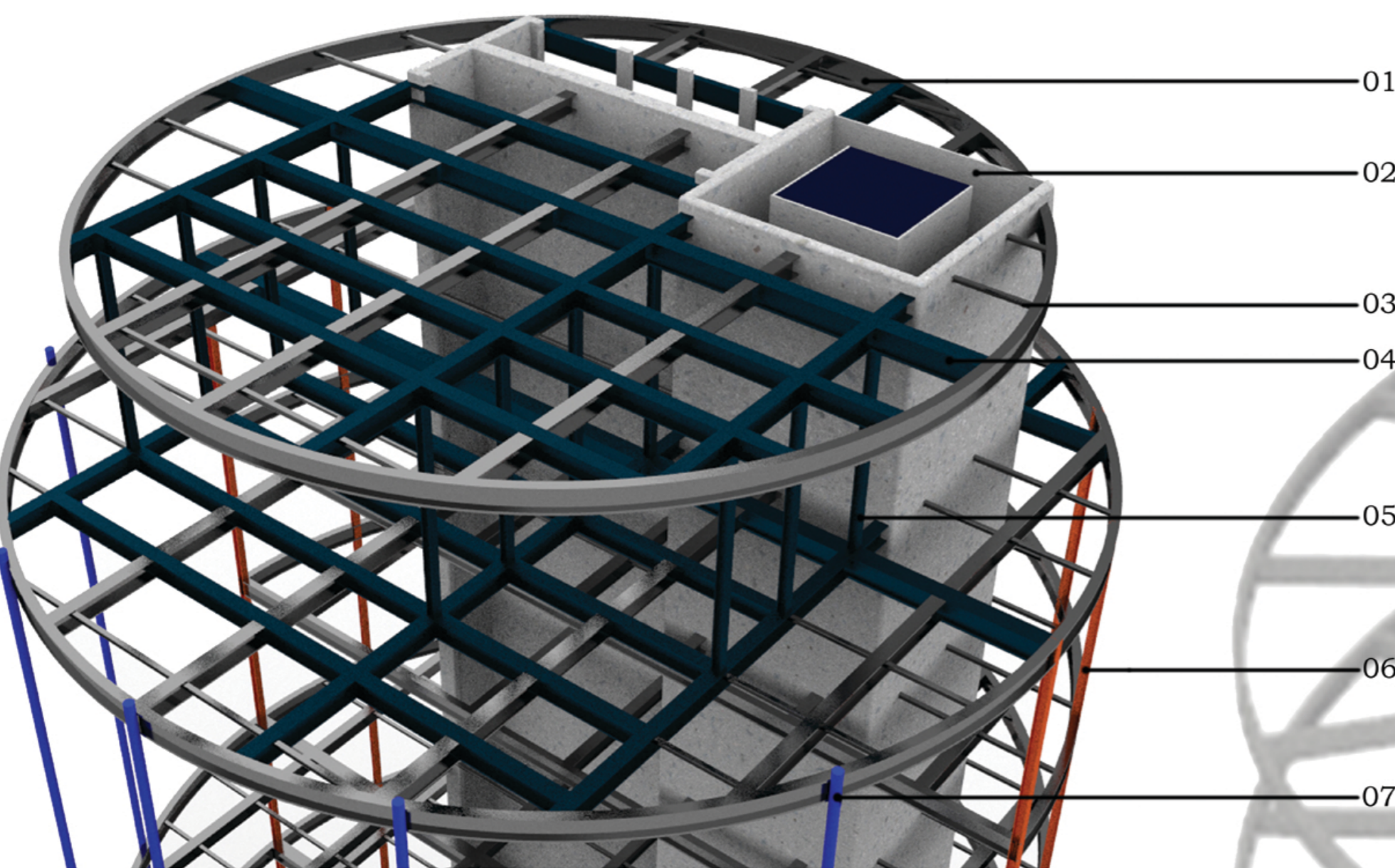
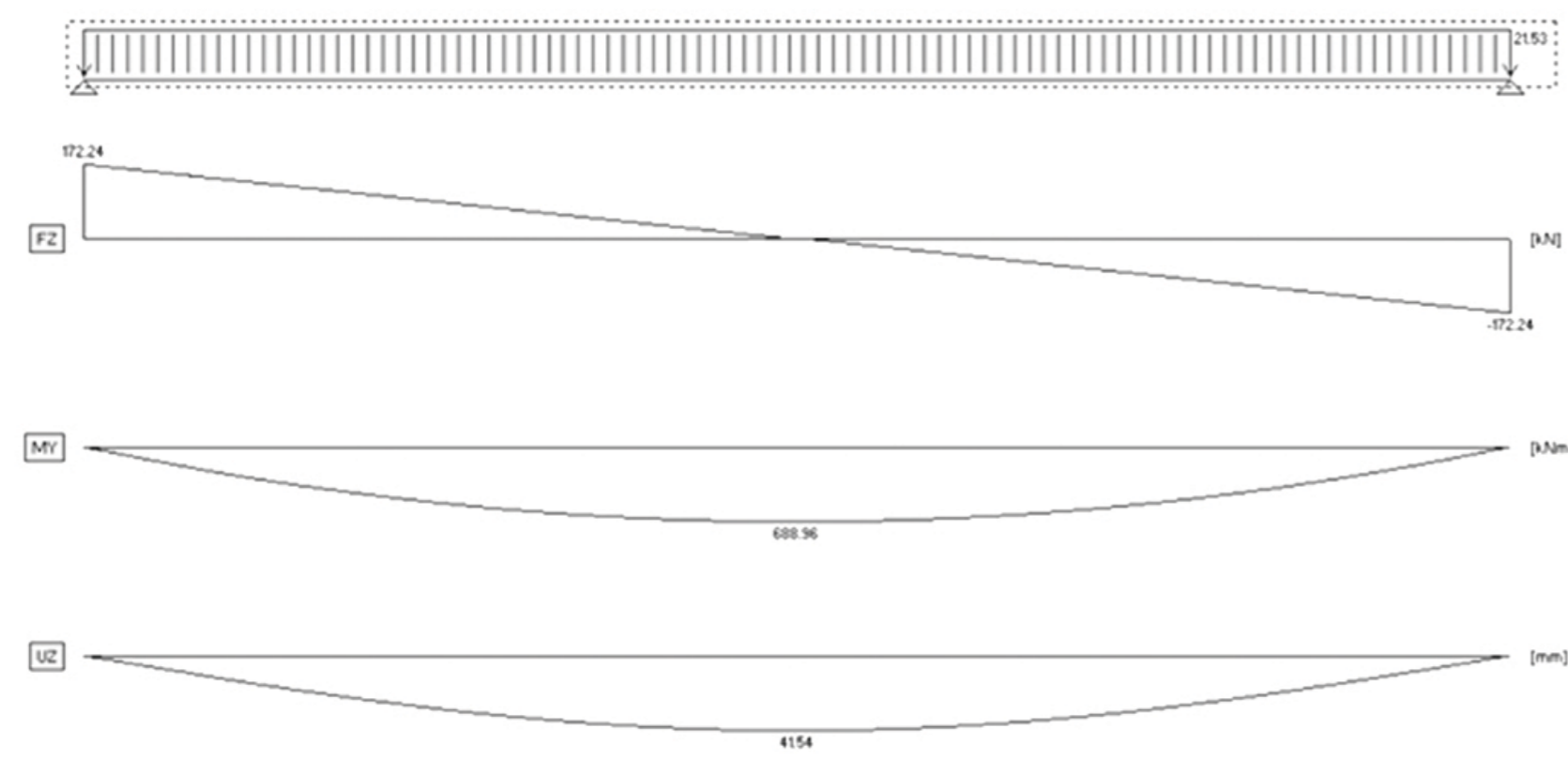
Bending moment primary beam :

Equivalent load (q<sub>sd</sub>) :  
 $q_{sd} = \gamma_{g1} * g_{1k} + \gamma_{g2} * g_{2k} + \gamma_{q1} * q_k + \gamma_{q2} * \psi * q_s$   
 = 1.3 \* 4.37 + 1.5 \* 4.31 + 1.5 \* 3  
 = 17.51 kN/m<sup>2</sup>

Med :  
 = q<sub>sd</sub> \* l<sup>2</sup> / 8  
 = 17.51 \* (10)<sup>2</sup> / 8  
 = 218.88

MR<sub>d</sub> :  
 = W<sub>pl</sub> \* f<sub>yk</sub> / γ<sub>m0</sub>  
 = 2884 \* 103 \* 355 / 1.05  
 = 976.06

Med / MR<sub>d</sub> < 1 → verified  
 218.88 / 976.06 = 0.22

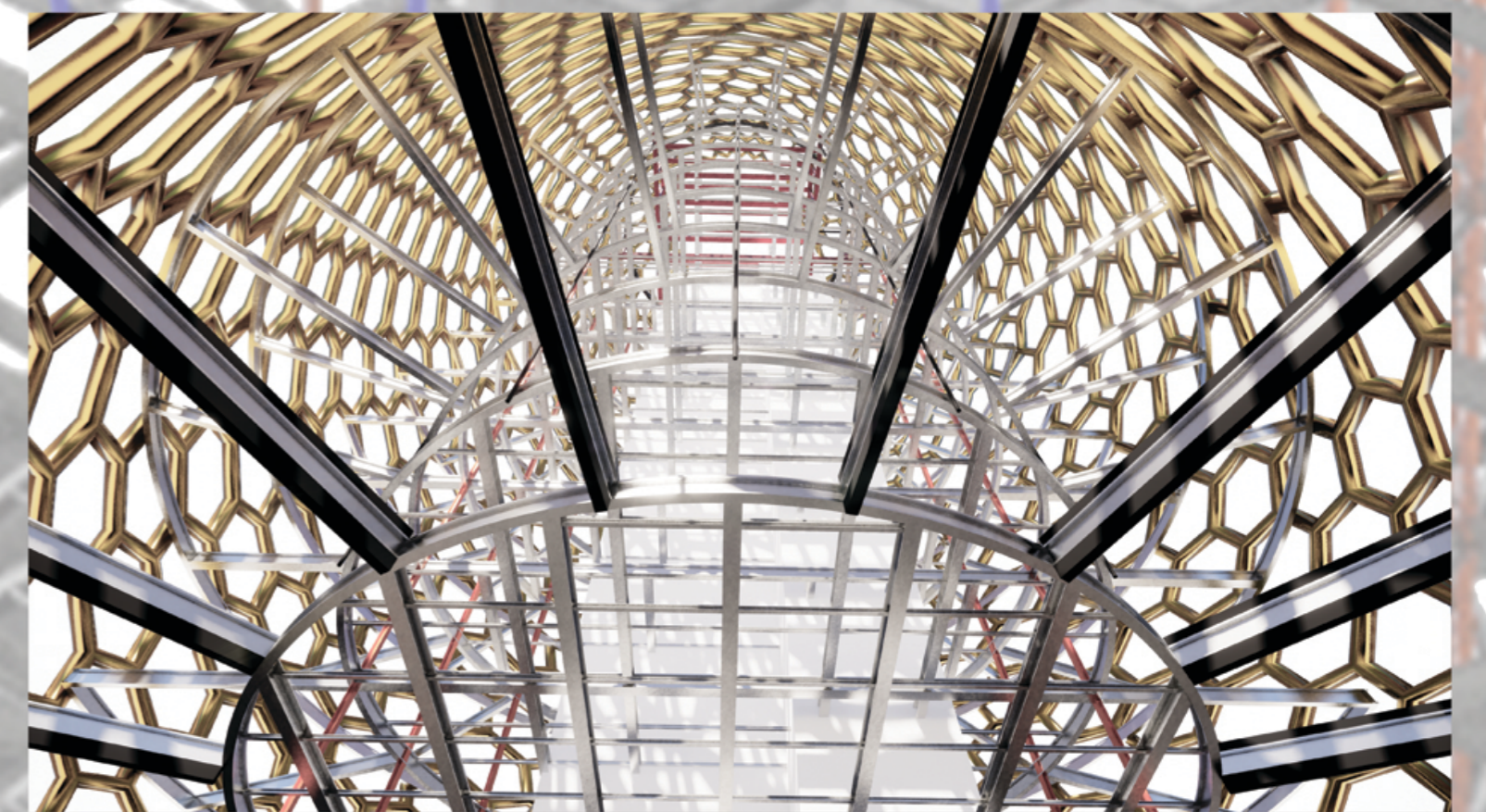
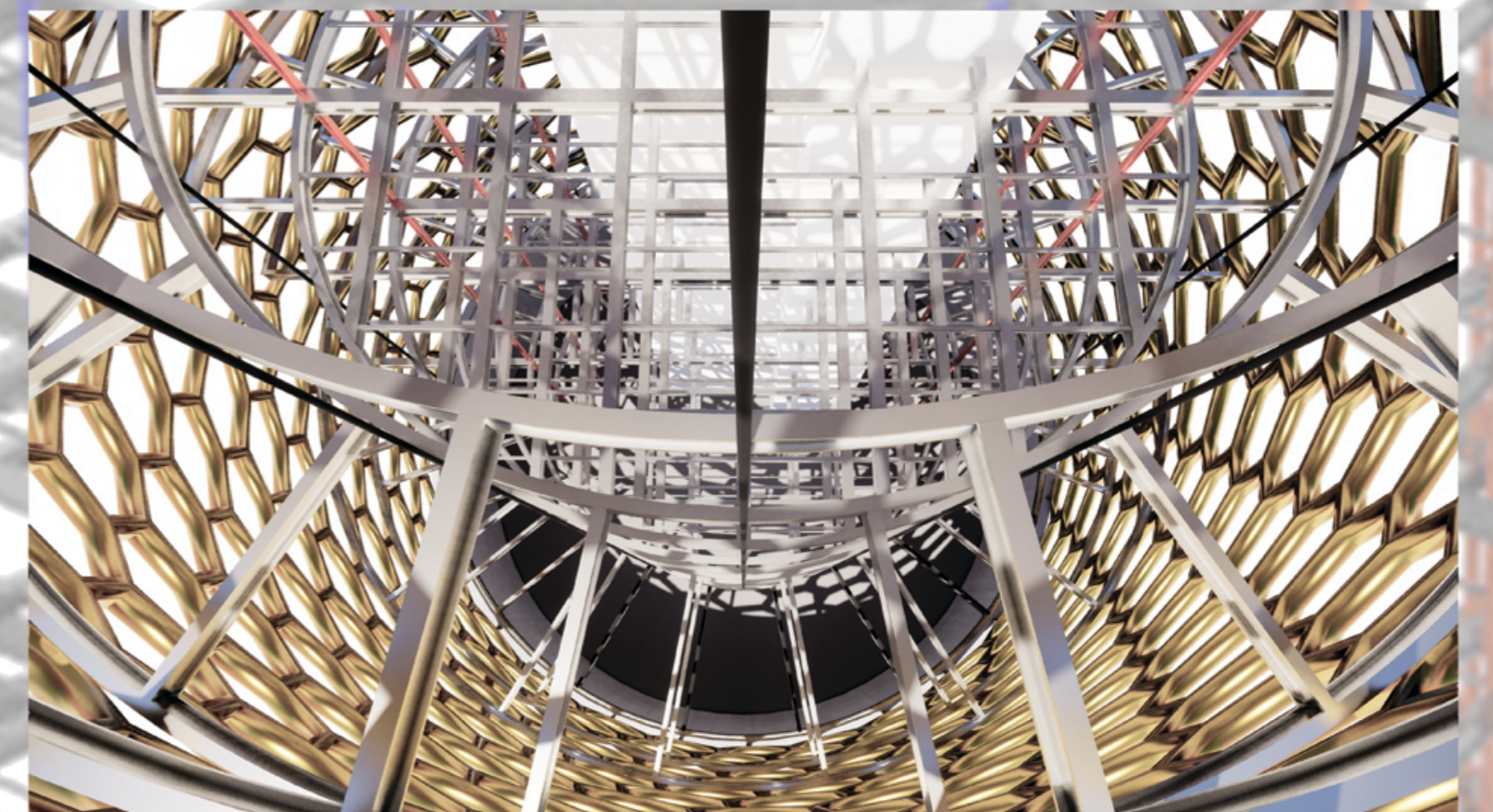


FACADE FRAME

PRIMARY & SECONDARY BEAMS

### COMPONENTS :

1. Primary Beam
2. Shear Wall
3. Secondary Beam
4. Vierendeel Beam
5. Vierendeel Column
6. MAin Column
7. Suspended Element



## Design of columns

Datas:  
 - h = 5 m  
 - A<sub>infl</sub> = 3.6 m \* 10 m  
 = 36 m<sup>2</sup>

Cross section selected:  
 HE 220 B  
 - A = 9100 mm<sup>2</sup>  
 - S355 → FE510  
 - σ<sub>adm</sub> = 240 N/mm<sup>2</sup>

Equivalent load (N) :  
 $N = (\gamma_{g1} * g_{1k}) + (\gamma_{g2} * g_{2k}) + (\gamma_{q1} * q_k) + (\gamma_{q2} * \psi * q_s) * (A_{infl} * n \text{ floors})$   
 = ((1.3 \* 5.05) + (1.5 \* 4.31) + (1.5 \* 3)) \* (3.6 \* 10 \* 10)  
 = 63072 kN/m<sup>2</sup>

σ<sub>max</sub> :  
 = N / A<sub>column</sub>  
 = 63072000 / 9100  
 = 6390.98

σ<sub>max</sub> / σ<sub>adm</sub> < 1 → verified  
 6390.98 / 240 = 26.63

l<sub>0</sub> = 1 \* 80%  
 = 500 cm \* 80%  
 = 400 cm

σ<sub>stressadm</sub> = 20

σ<sub>stressmax</sub> = 10/a  
 = 400 / 22  
 = 18.18

σ<sub>stressmax</sub> / σ<sub>stressadm</sub> < 1 → verified  
 18.18 / 20 = 0.90

## Design of tension element (suspended slab)

Dead load (g):  
 - g<sub>1k</sub> = ribbed slab self-weight + secondary beam self-weight  
 = 2.65 + 0.20  
 = 2.85 kN/m<sup>2</sup>  
 - g<sub>2k</sub> = not structural dead loads  
 = 5.18 kN/m<sup>2</sup>

Live load (qk):  
 - occupancy load = 5 kN/m<sup>2</sup>  
 Total load (q):

$q_{sd} = (\gamma_{g1} * g_{1k} + \gamma_{g2} * g_{2k} + \gamma_{q1} * q_k + \gamma_{q2} * \psi * q_s) * N_{\text{floors suspended}}$   
 = (1.3 \* 2.85 + 1.5 \* 5.18 + 1.5 \* 5) \* 9  
 = 170.73 kN/m<sup>2</sup>

Area slab:  
 A<sub>slab</sub> = 400 m<sup>2</sup>  
 (\*considering bigger area)

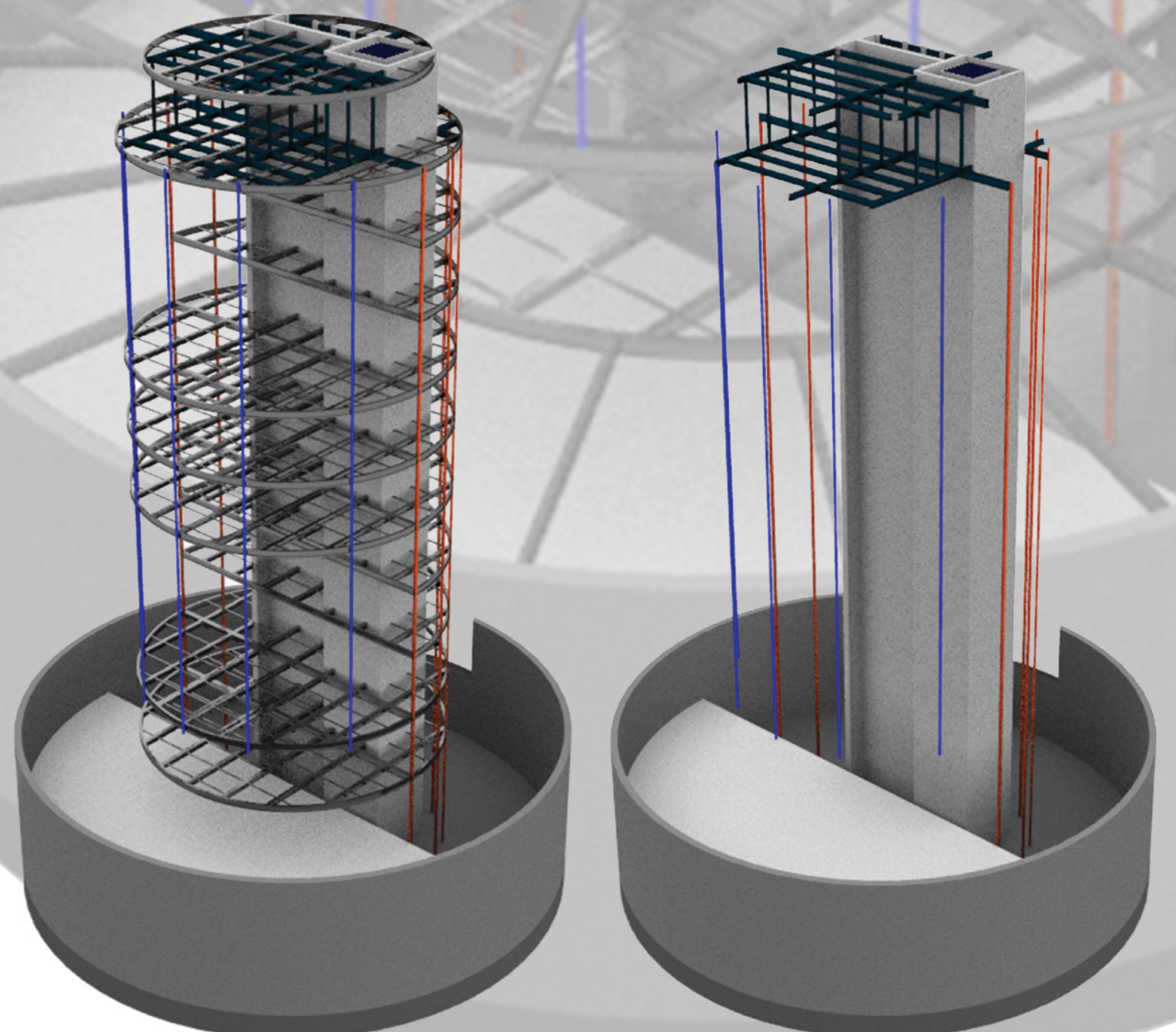
Safety coefficient:  
 f<sub>yd</sub> = f<sub>y</sub> / γ<sub>m</sub>  
 = 355 / 1.05  
 = 33.80 kN/cm<sup>2</sup>

Axial load:  
 N<sub>d</sub> = q<sub>sd</sub> \* A<sub>slab</sub>  
 = 170.73 \* 400  
 = 68292 kN

Area of cable:  
 A<sub>ULS</sub> = N / f<sub>yd</sub>  
 = 68292 / 33.80  
 = 20.20 cm<sup>2</sup>

Elongation:  
 $\Delta_{tot} = \sum_{i=1}^n N_i * l_i / E * A_{profile}$   
 = 9 \* ((2.85 + 5.18) \* 9) \* 45 / 210000 \* 15.6  
 = 9 \* 117.27 \* 45 / 210000 \* 15.6  
 = 14.90 mm

Δ<sub>adm</sub> = 50mm  
 Δ<sub>tot</sub> / Δ<sub>adm</sub> < 1 → verified  
 14.90 / 50 = 0.29



VIERENDEEL TRUSS

COLUMNS AND SHEAR WALLS

