BEACON ****

Affordable housing allows for a healthy economy while enjoying decent dwelling. It revitalises and maintains neighbourhoods by increasing security, business, integration and providing families with a sustainable lifestyle.

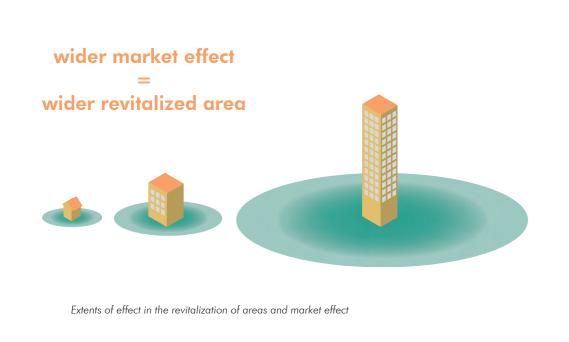
Yet housing is not just housing anymore! While the change started years prior, the beginning of the decade demonstrated that a home is not just for living. It is the place for learning, working, exercising, a scenario for socializing and community-building. It is this how the idea of this project arises. An amount of square footage -which would otherwise be used for activities that benefit from social engagementis taken from each apartment and placed in semi-common areas called "shared-ownership spaces". It is here where owners can encounter each other without relinquishing ownership of areas, space, functions or even momentaneous privacy. Encouraged by the diversity and the love for art and culture of Toronto, the program of these areas is knit to rentable public places that call for dancing, fitness, film-making, cooking and language-learning.

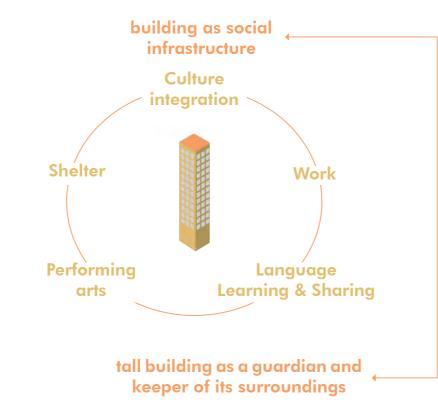


ANALYSIS

TORONTO'S SOCIAL QUALITIES

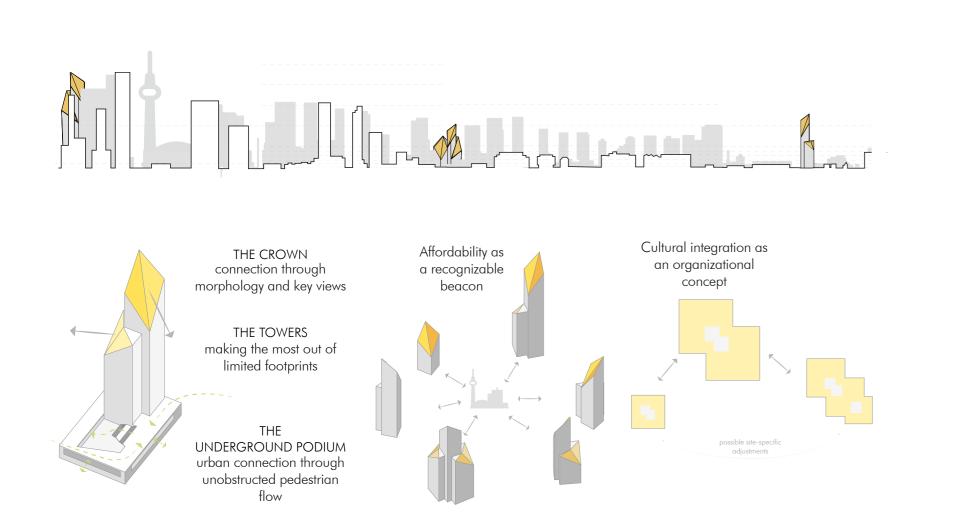


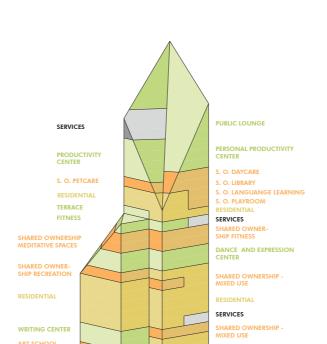




PROGRAM

CONCEPT





external temporary

accomodations

Traditional Programatic

Separation

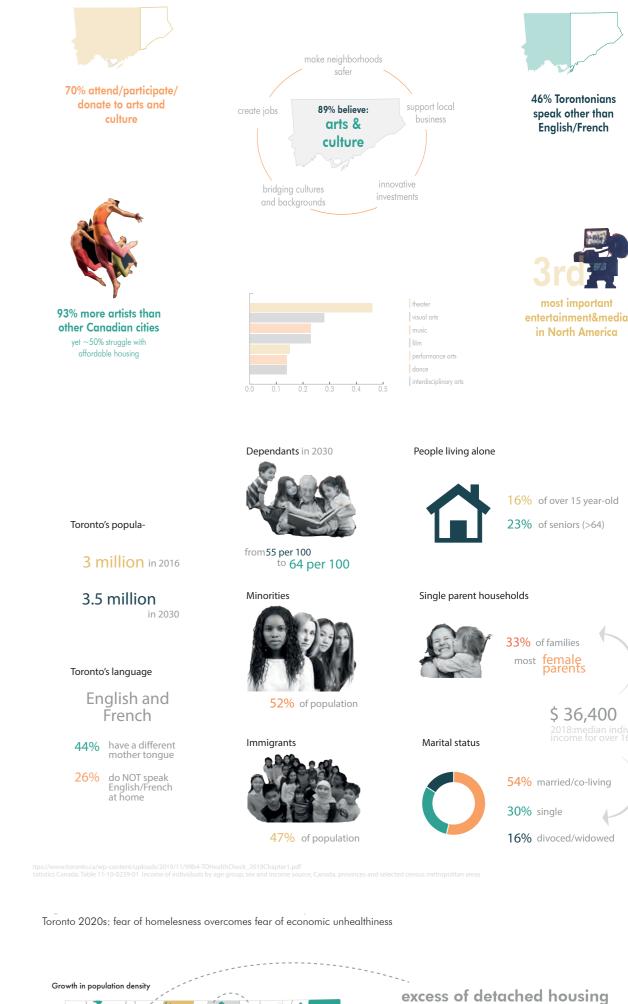
new

shared

ownership

New Programatic

Integration

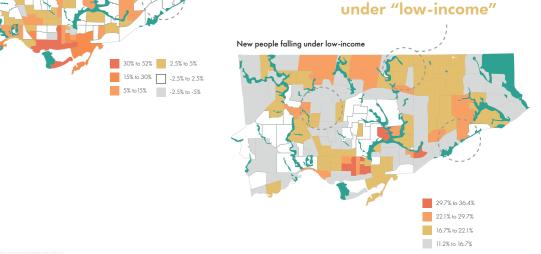


(no vertical density)

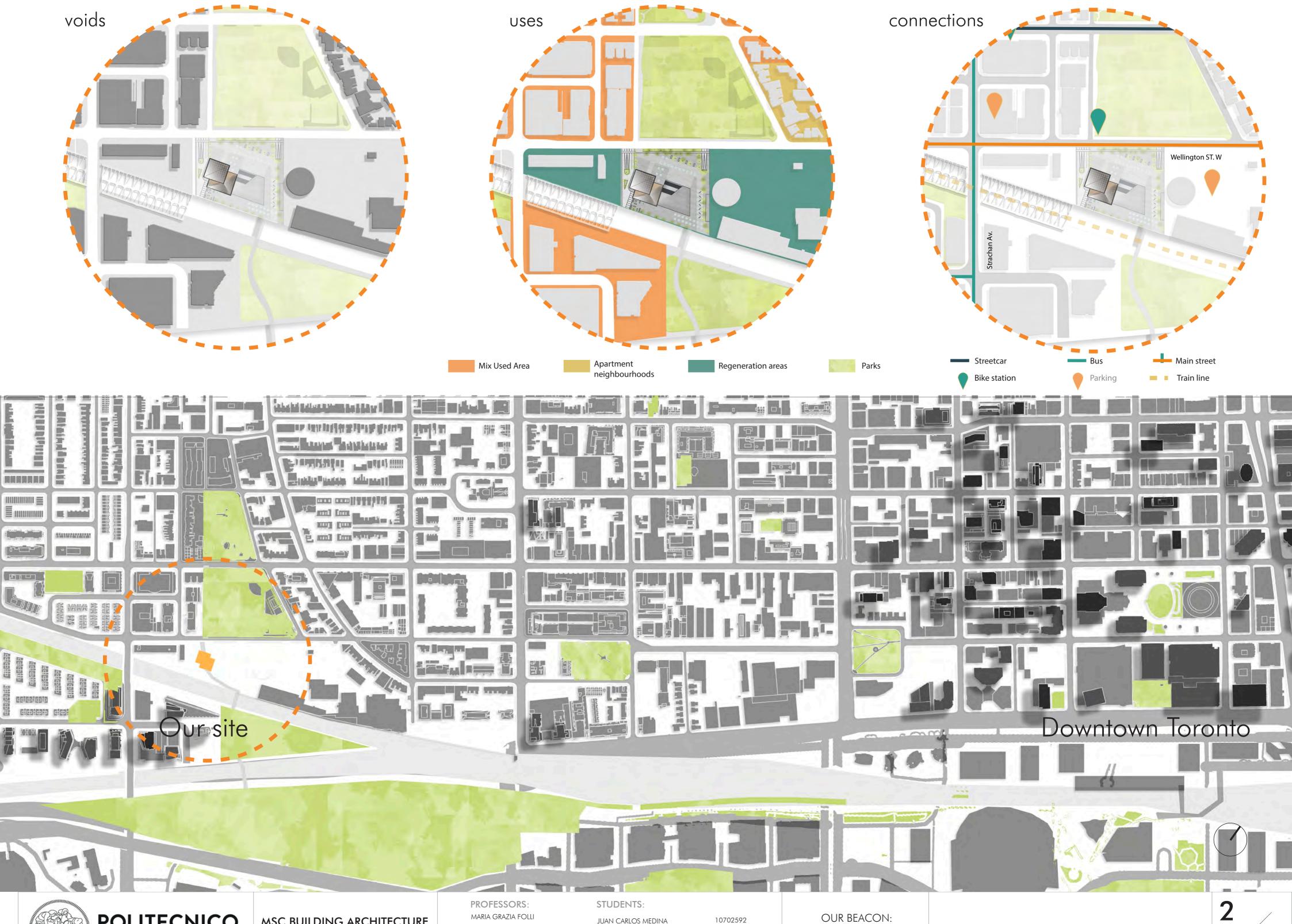
= more people falling

26





OUR SITE



POLITECNICO MILANO 1863

MSC BUILDING ARCHITECTURE THESIS PROFESSORS: MARIA GRAZIA FOLLI CORRADO PECORA GIOVANNI DOTELLI FRANCESCO ROMANO MARCO IMPERADORI

JUAN CARLOS MEDINA MARIA JOSE MONTERO DIANA MARISOL NARVAEZ

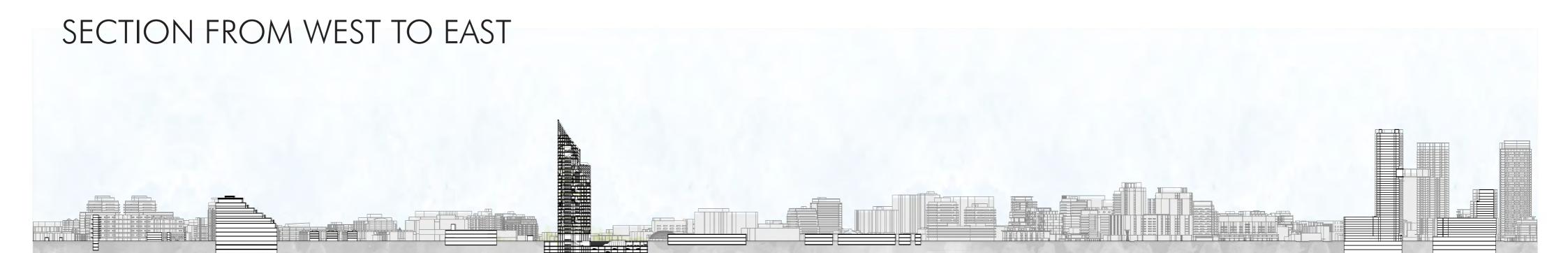
10712731

10704376

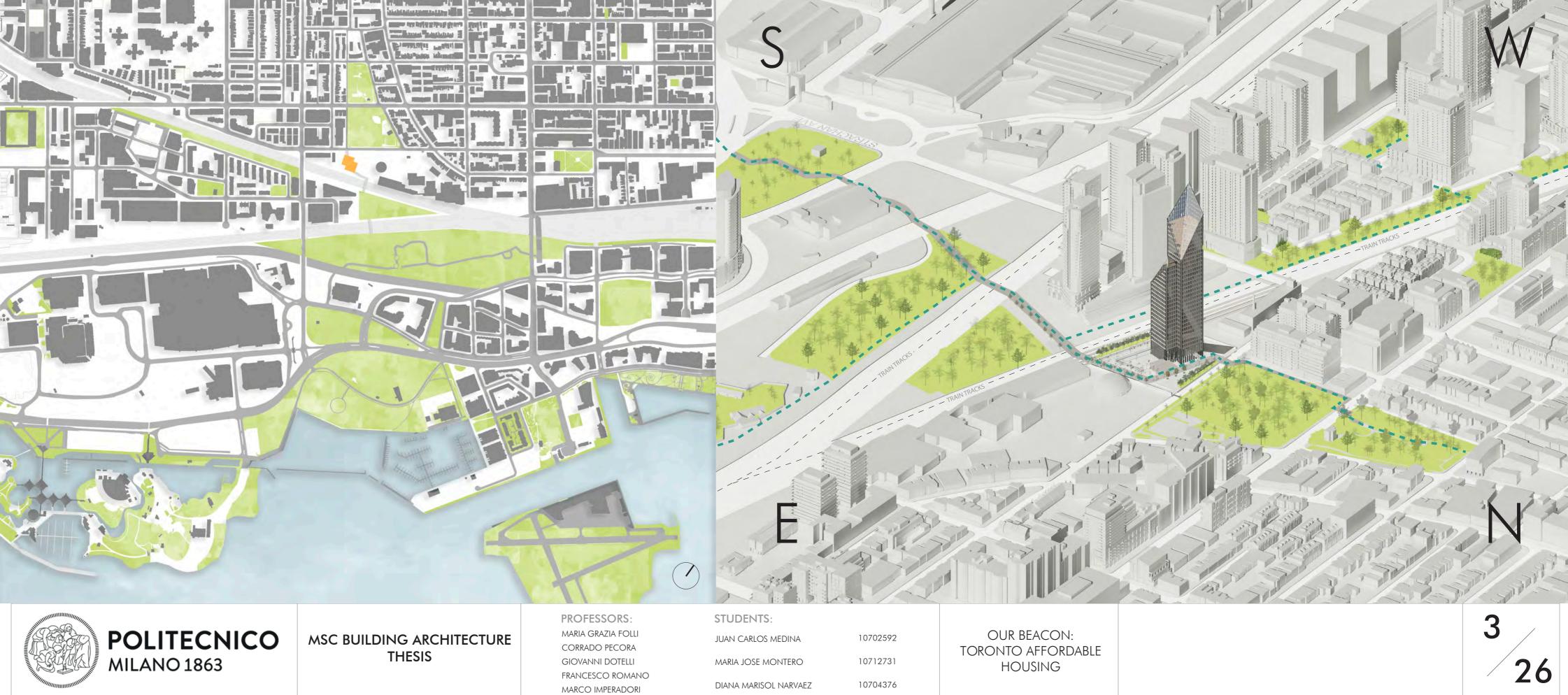
OUR BEACON: TORONTO AFFORDABLE HOUSING SITE

ELEVATION FROM WEST TO EAST

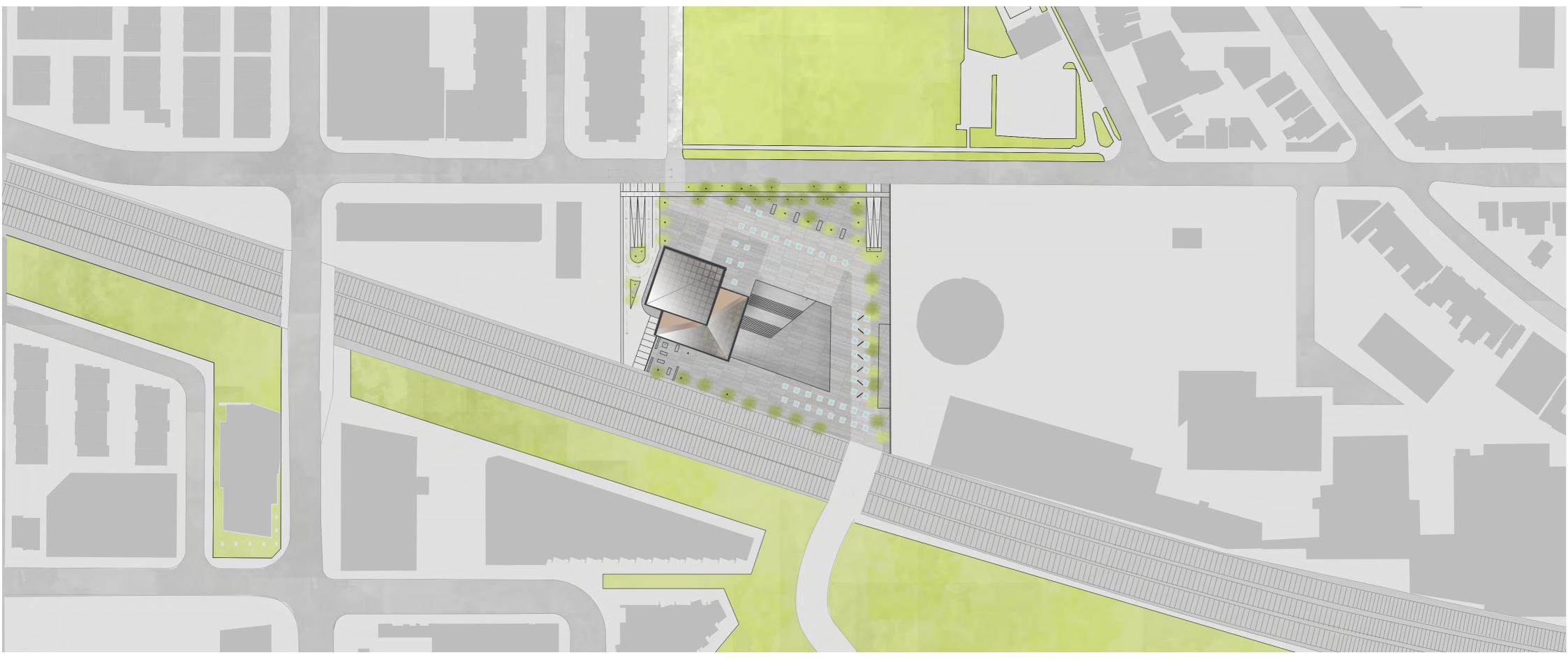








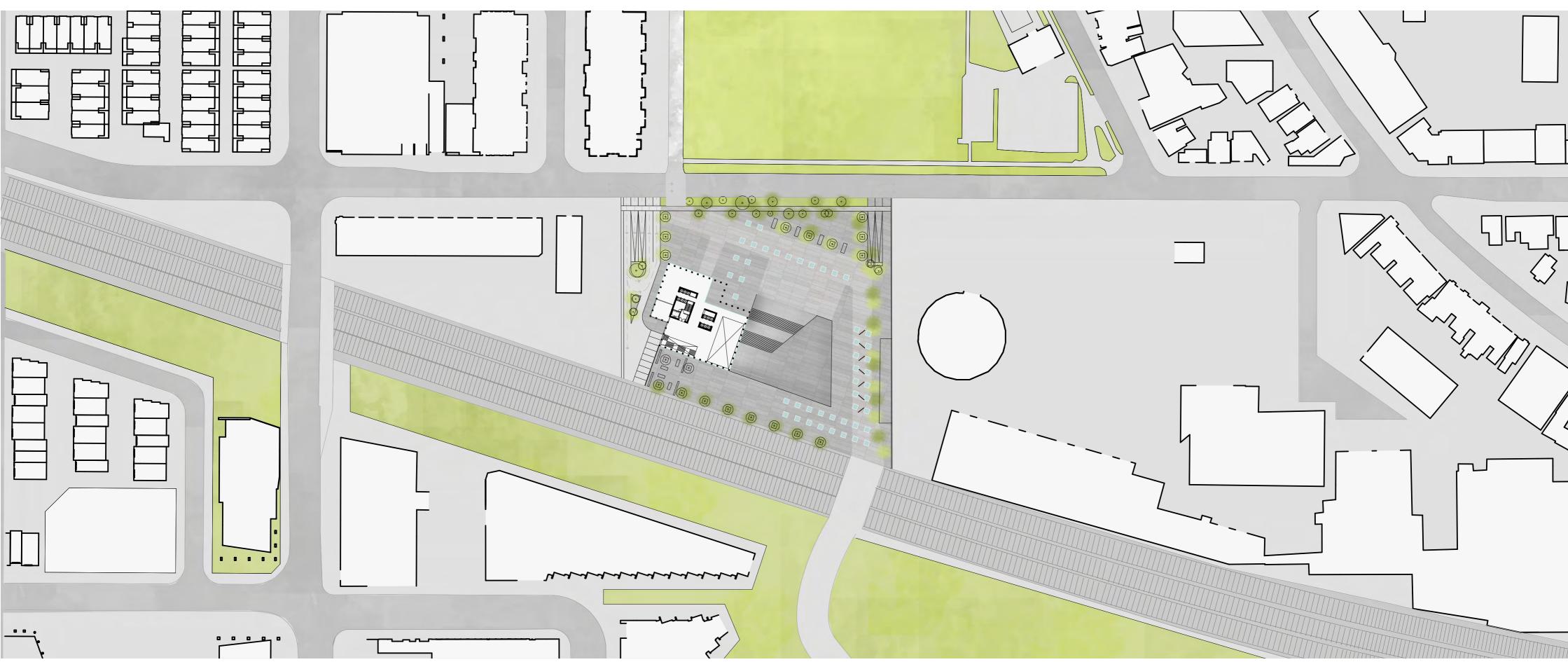
GROUND FLOOR



SITE

SITE PLAN





VIEW FROM PLAZA



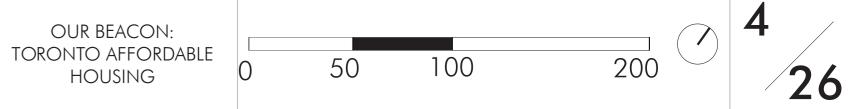




MSC BUILDING ARCHITECTURE THESIS

PROFESSORS: MARIA GRAZIA FOLLI CORRADO PECORA GIOVANNI DOTELLI FRANCESCO ROMANO MARCO IMPERADORI

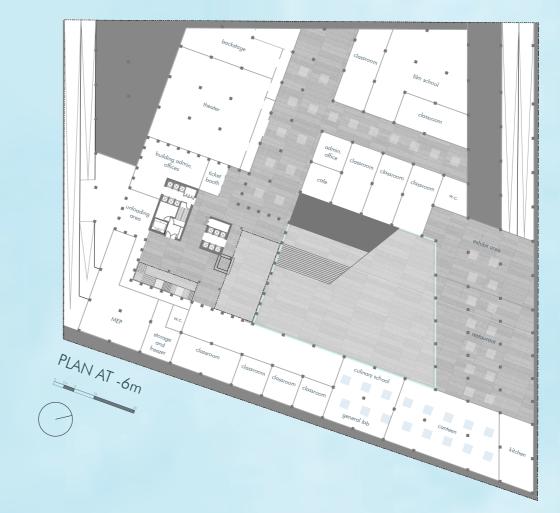
STUDENTS: 10702592 JUAN CARLOS MEDINA MARIA JOSE MONTERO 10712731 10704376 DIANA MARISOL NARVAEZ



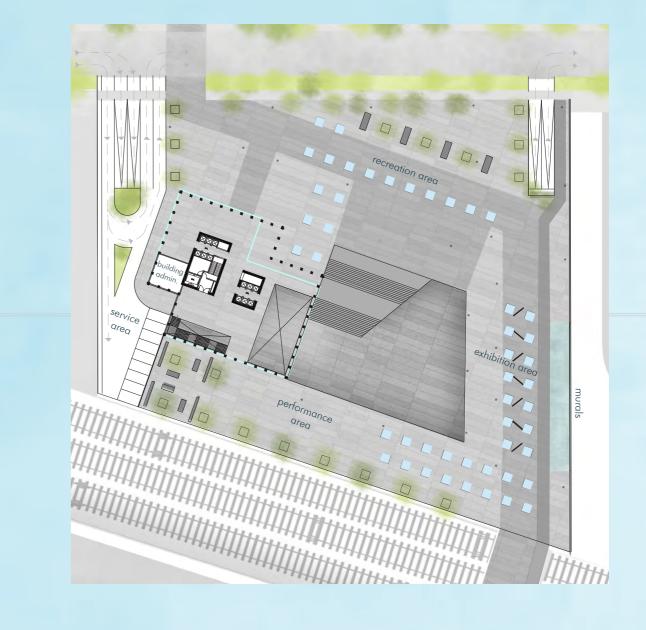
SECTION AND PUBLIC PLAZA PLANS

NORTH-SOUTH SECTION





Underground floor



Ground floor



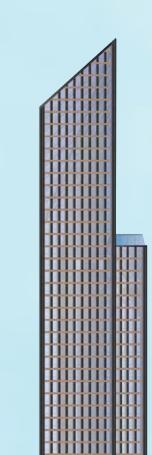


SECTION AND ELEVATIONS

WEST-EAST SECTION







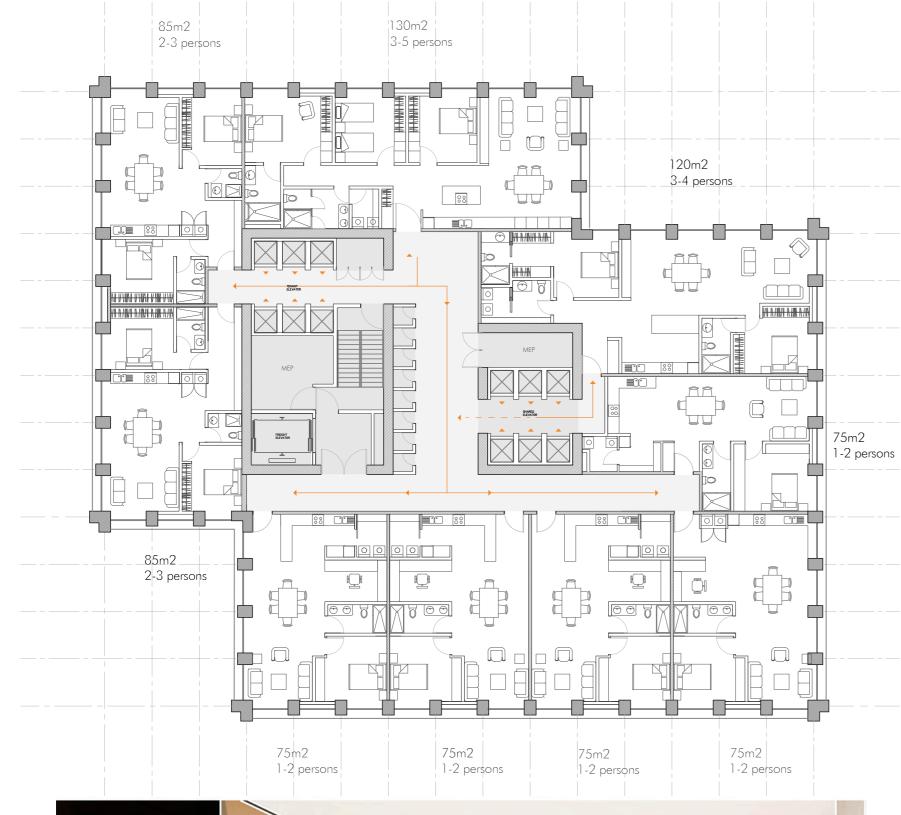
WEST

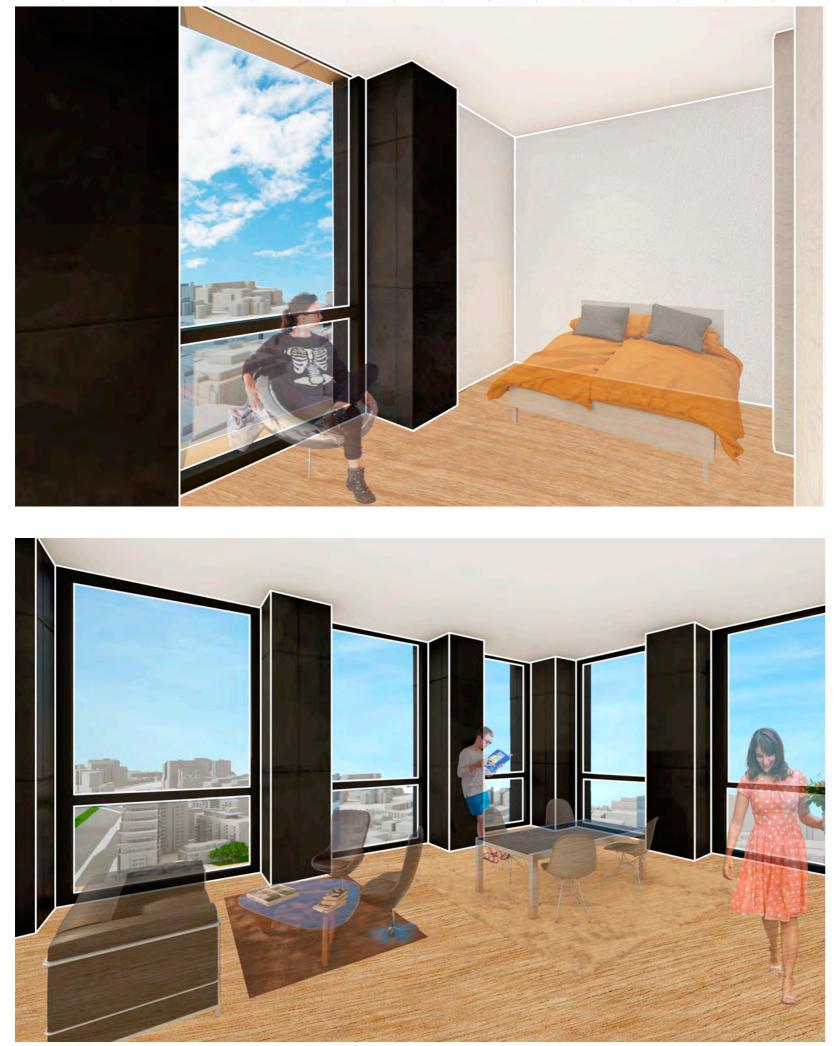
SOUTH



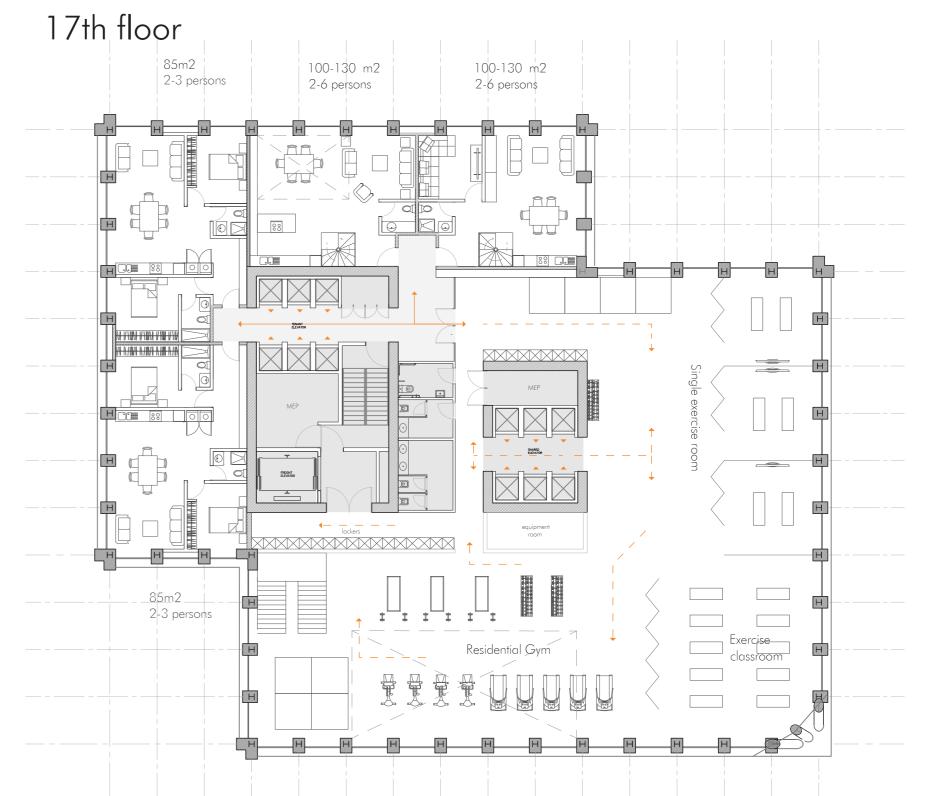
PLANS

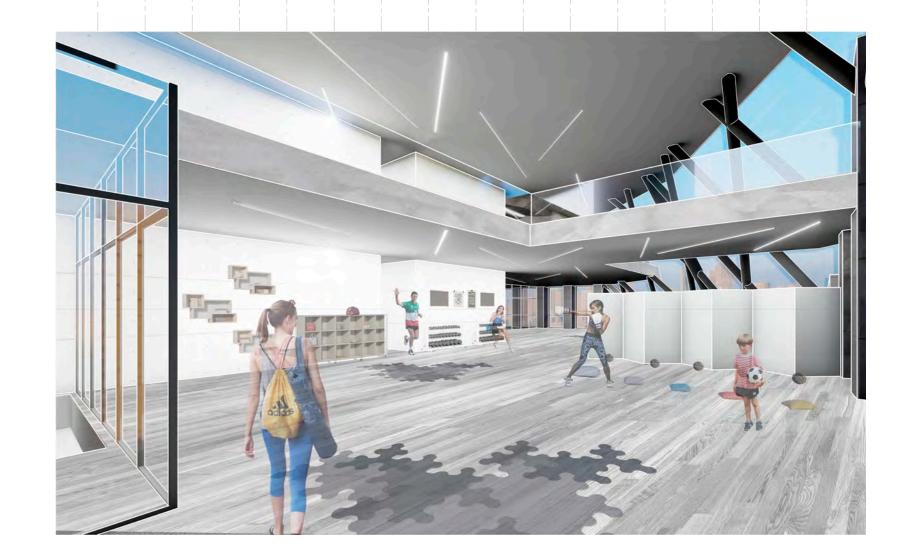
RESIDENTIAL





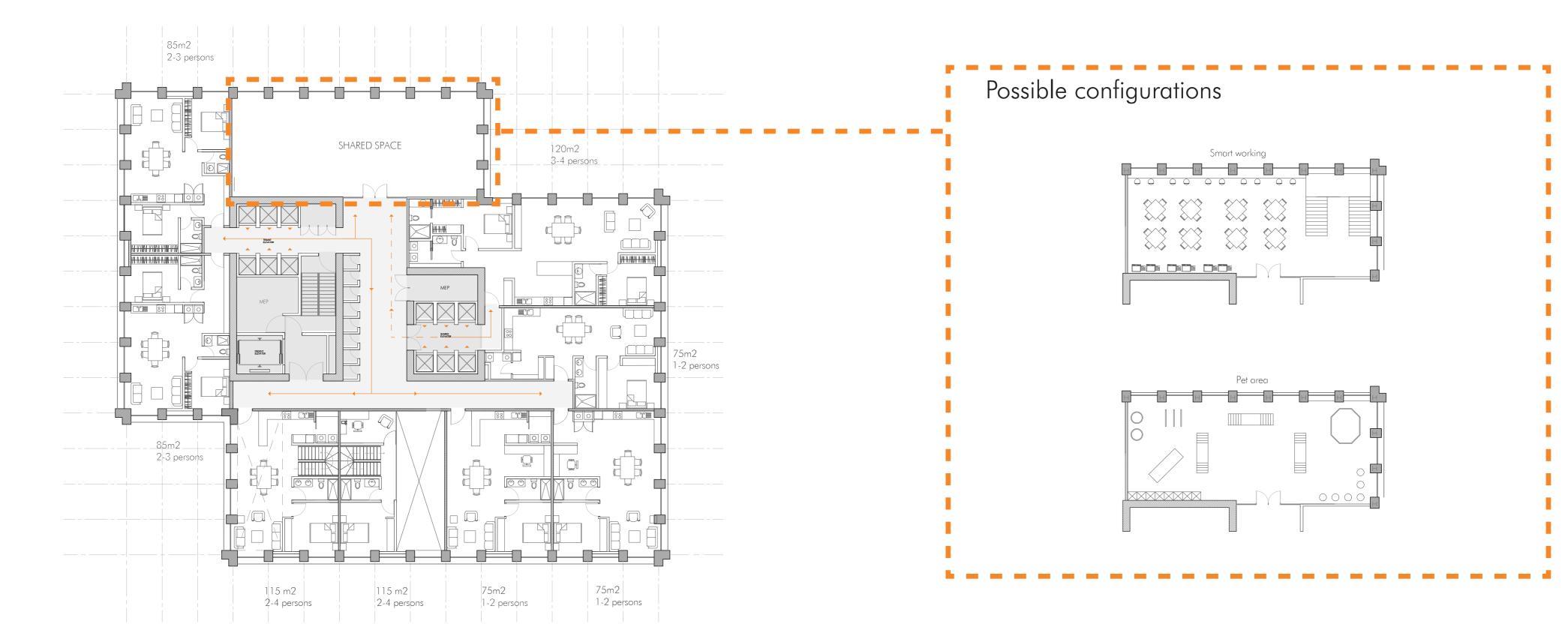
RESIDENTIAL/ GYM





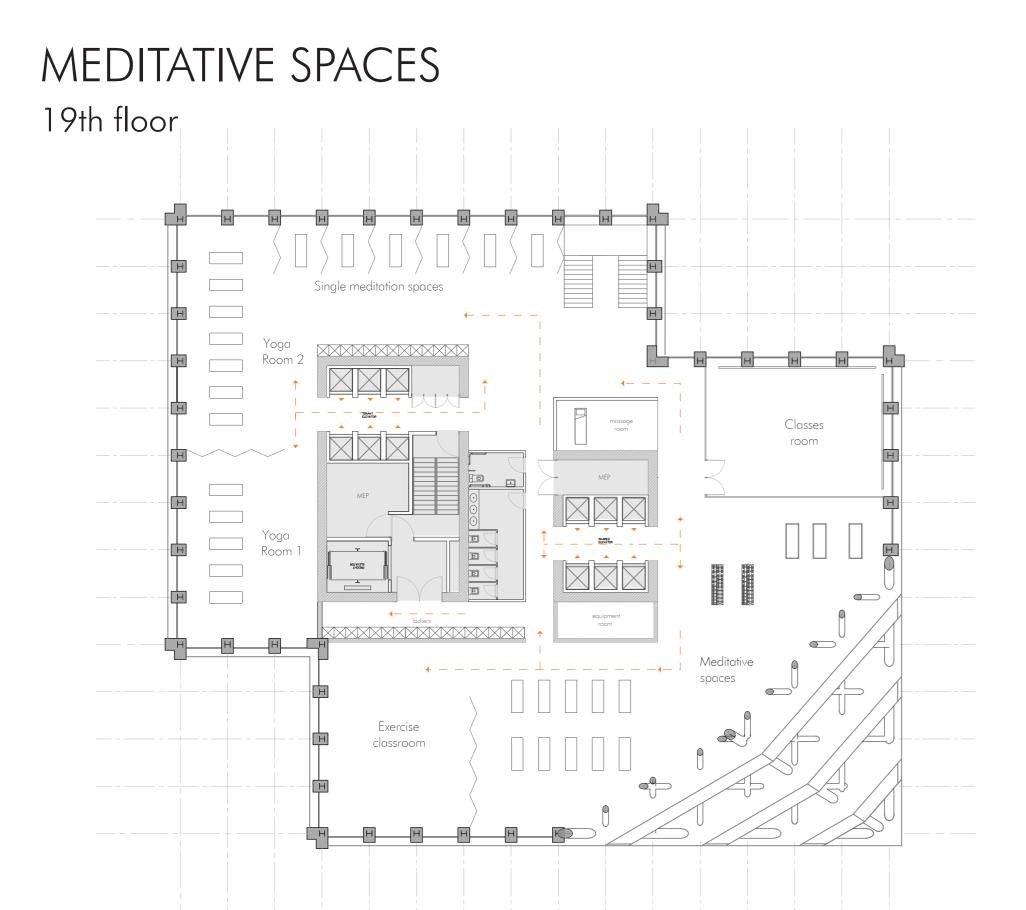
RESIDENTIAL/ SHARED SPACES



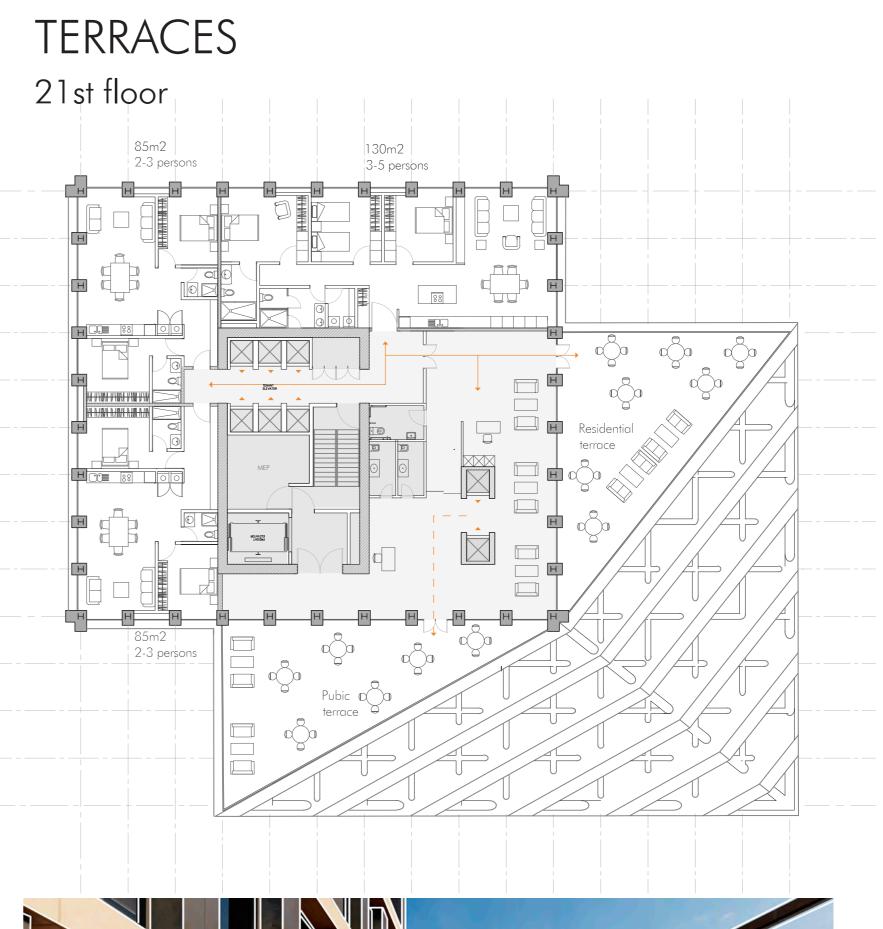




PLANS

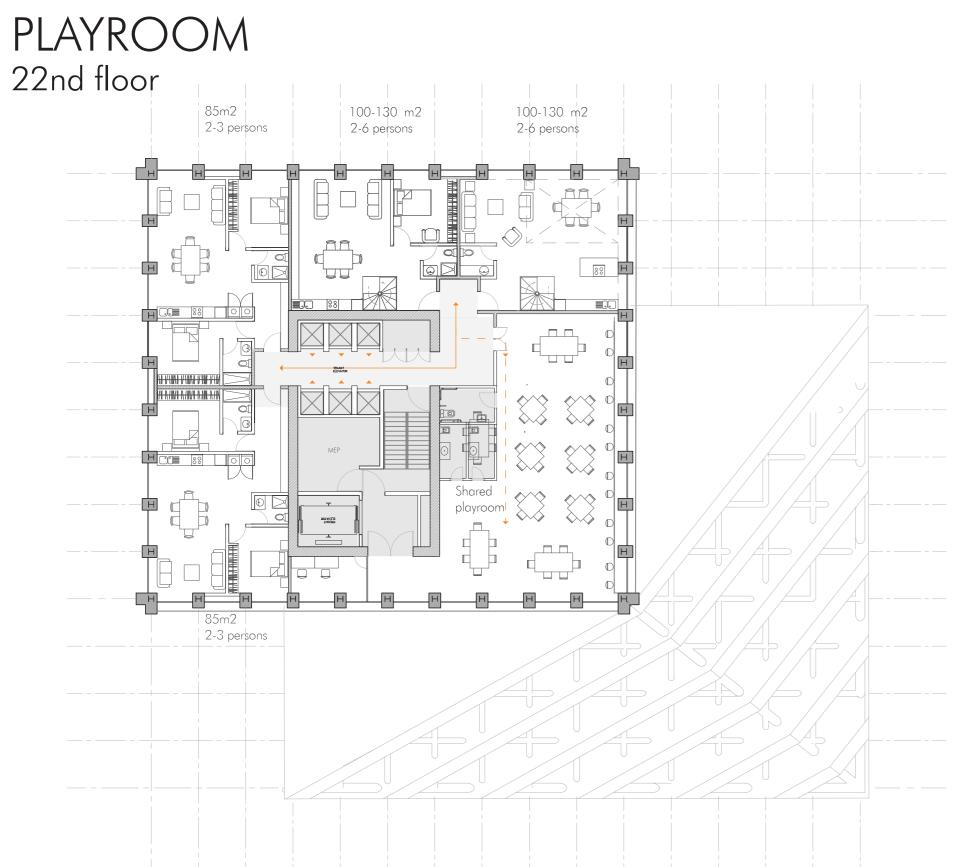




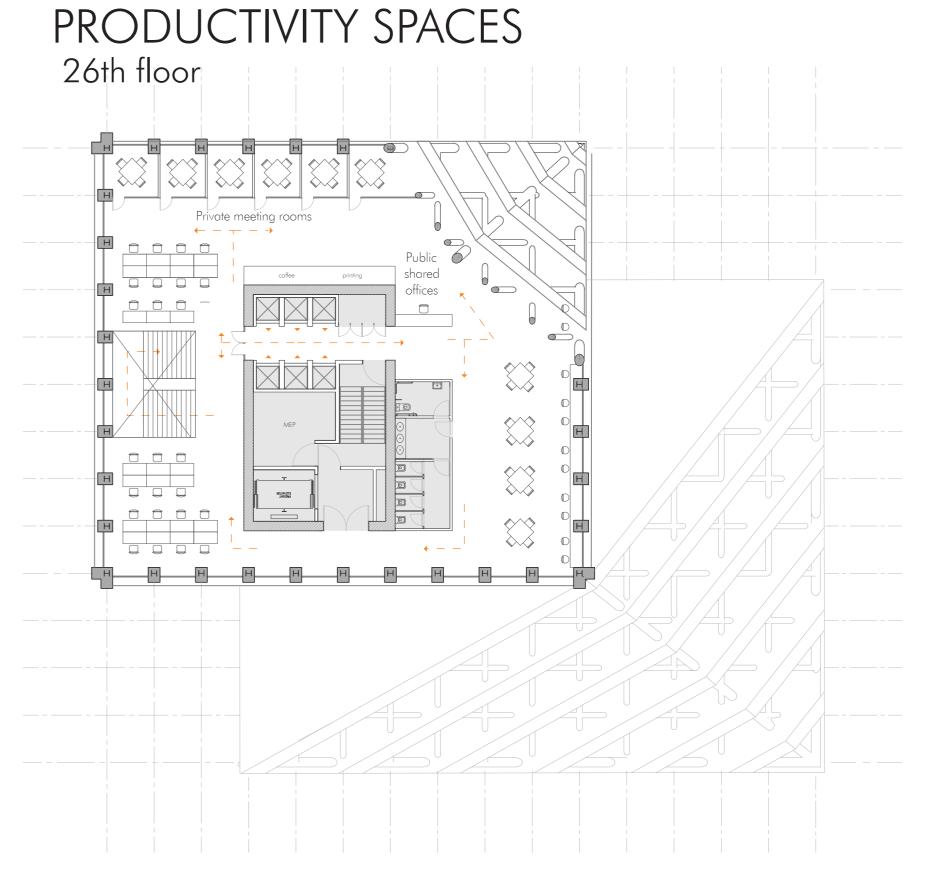










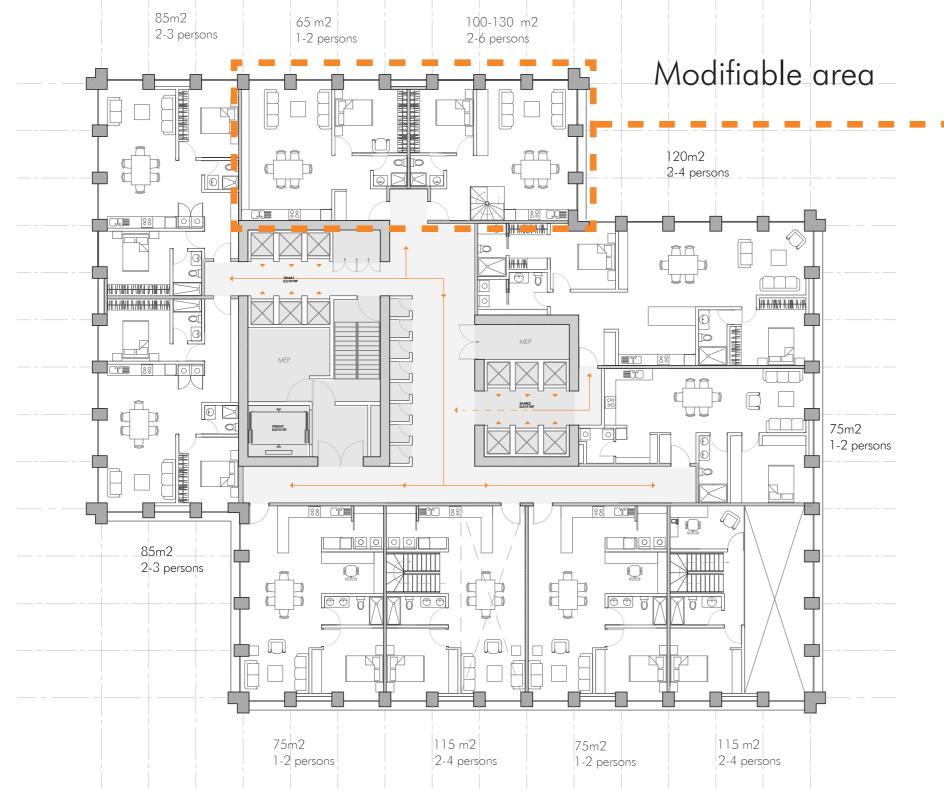


| POLITECNICO MILANO 1863 MILANO 1863 | E PROFESSORS: MARIA GRAZIA FOLLI CORRADO PECORA GIOVANNI DOTELLI FRANCESCO ROMANO MARCO IMPERADORI | STUDENTS: JUAN CARLOS MEDINA MARIA JOSE MONTERO DIANA MARISOL NARVAEZ | 10702592 10712731 10704376 | OUR BEACON: TORONTO AFFORDABLE HOUSING | 1m 5m 10m | 8 26 | |
|---|---|---|----------------------------------|--|-----------|---------|--|
|---|---|---|----------------------------------|--|-----------|---------|--|

DOUBLE HEIGHT APPARTMENTS

POSSIBLE FLOOR VARIATIONS

Possible in all residential levels



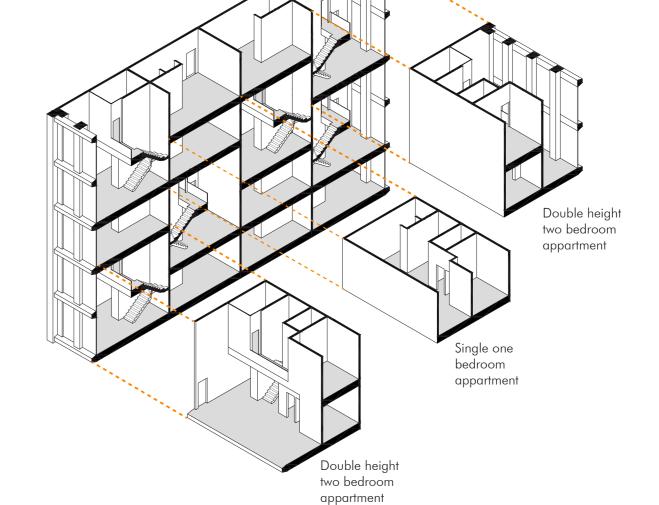


Configurations diagram



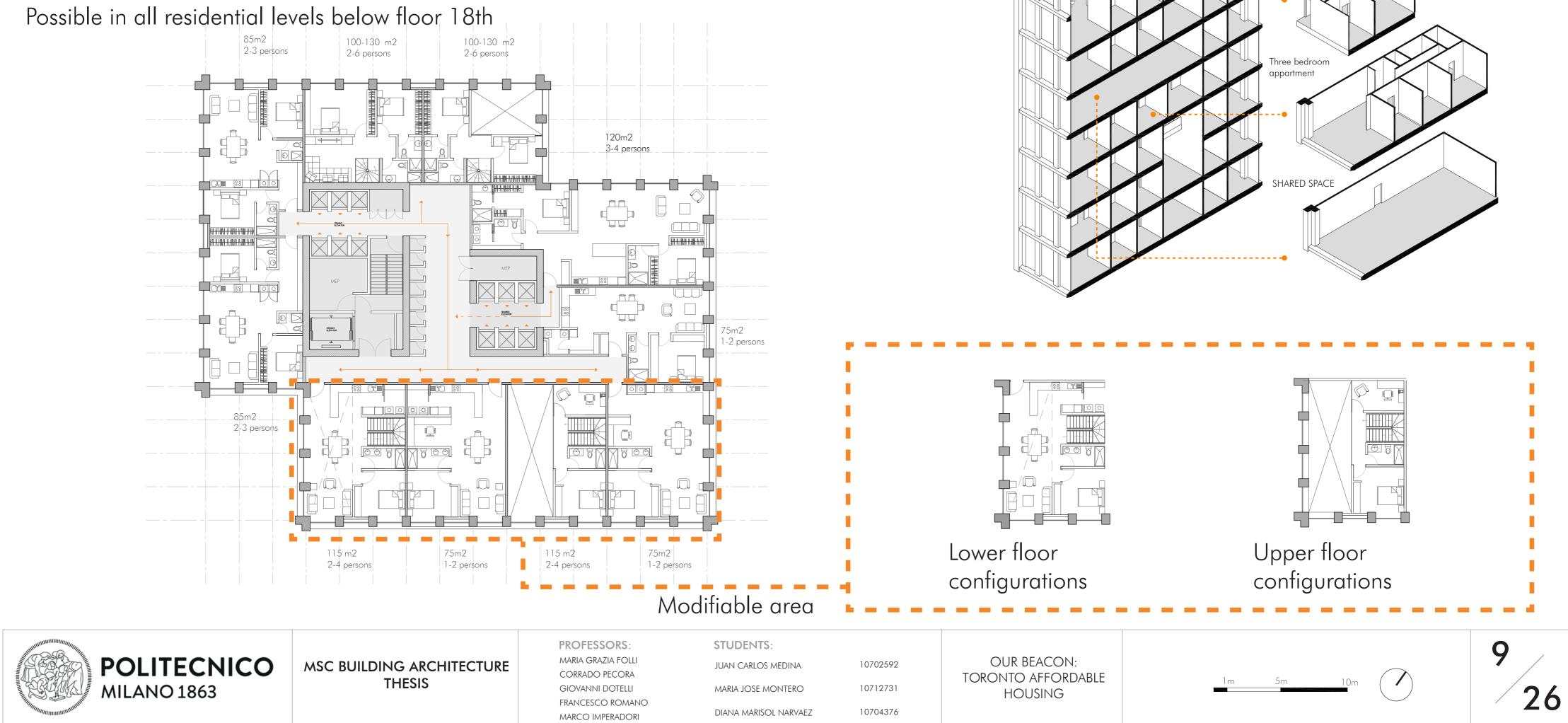
Interior views

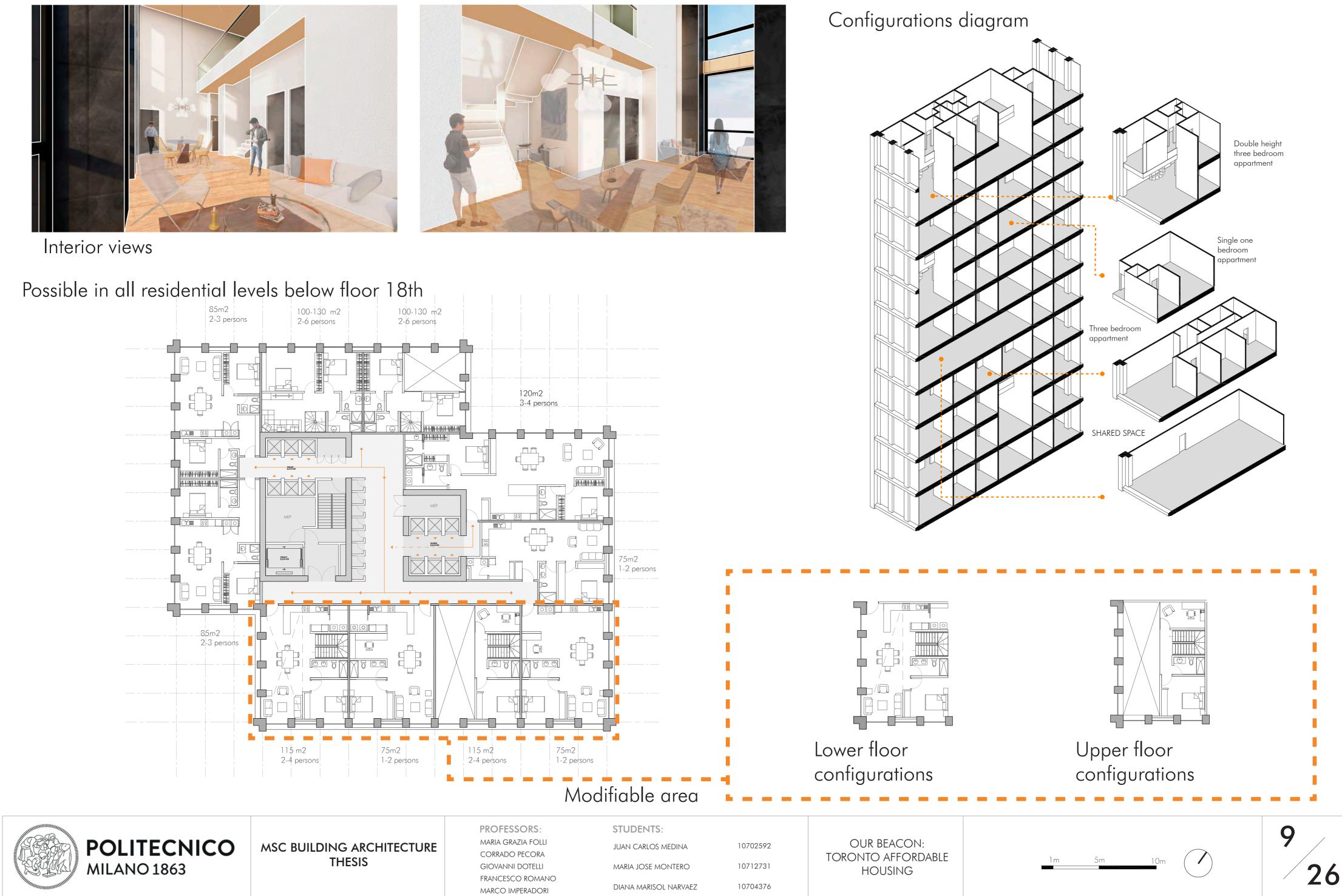






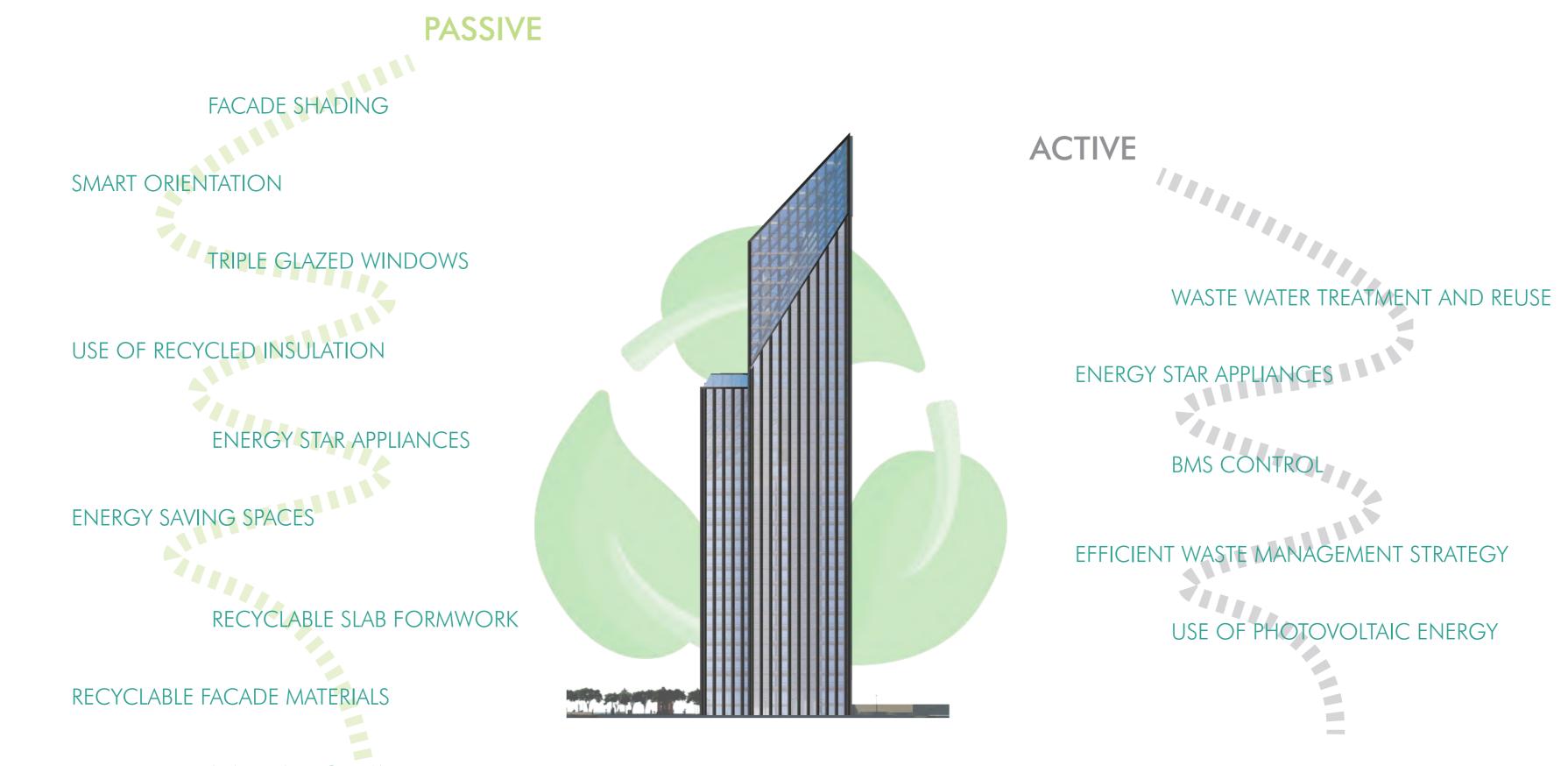








SUSTAINABILITY PRINCIPLES

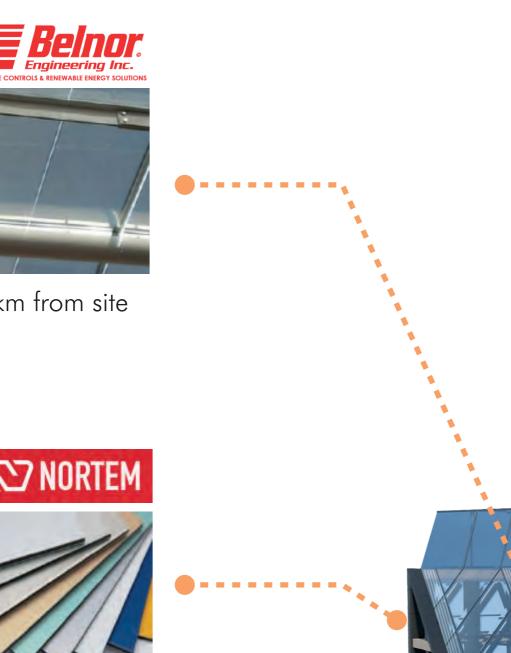


NATURAL LIGHT AT THE



MATERIAL PALETTE

GLASS













MATERIAL PROPERTIES/ PRODUCERS



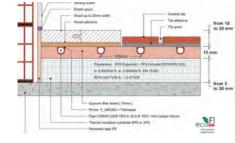
| Programme: | The International EPD" System, w | vww.environdec.com |
|-------------------------------|----------------------------------|--------------------|
| Programme operator: | EPD International AB | |
| EPD registration number: | S-P-03087 | FPD |
| Publication date: | 2021-03-19 | |
| Valid until: | 2026-03-18 | LED PLATIENM |
| Scope of the EPD [®] | Global | EN 15804 VERIFIED |



- The INTERPLAST product declared in this EPD is the "EcoFloor Plus" system which combines a special gypsum fiberboard with under floor heating system. This new low profile, dry screed under-floor heating is designed and developed for higher energy efficiency and water savings. The analyzed product system includes:
- Thermal insulation
- Intermainsulation
 Gypsum fiberboard
 Piping system: PE-RT or PEX Ø10 x 1,1mm pipe which is utilized to transport hot and

cold water for underfloor heating applications. Other components (filling, primer, perimetric tape, pipe fittings and manifolds)

arity of EcoFloor allows for flexibility both in terms of insulation layer thickness, o



Advantages of EcoFloor Plu

 System height from 3.2 to 5cm including the final floor. Basic feature of the system i system neight from s, to stim including the man hour, basic reactive of the system in the special gypsum fiberboards which are produced under pressure from specia gypsum which is reinforced with cellulose fibers and specially processed with hydrophobic additives for moisture resistance · Ideal system for insulating building floors from air carried sounds · Ability of placing any final floor · Ideal system for old and new residence



| IMPACT RESISTANCE | BY DUPONT N | NETHOD | ALPOLIC [®] | /PE | | PRODUCT TO | DLERANO | E | |
|--|---------------------|---------------|-----------------------|----------------------|----------------------|------------------|-------------|-----------|---------------------|
| | | | DENT DEPTH (x10-2 IN) | | Width: | ± 0.08* (2mm) | | | |
| STEEL BALL | HEIGHT | | 3MM | 4MM | 6MM | Length: | ± 0.16* (| 4mm) | |
| | | | .118" | .157" | .236" | Thickness: | 3mm: | ± 0. | 008" (0.2mm) |
| 1.10 lb | 20 in | | 6.30 | 5.51 | 3.15 | | 4mm: | ± 0. | 008" (0.2mm) |
| 2.20 lb | 12 in | | 7.87 | 6.69 | 3.93 | | ómm: | ± 0. | 012" (0.3mm) |
| 2.20 lb | 20 in | | 10.23 | 9.05 | 5.90 | Bow: | maximum | 0.5% o | f length and/or w |
| | | | | | | Squareness Ma | ximium | 0.2 | !* (5mm) |
| BOND INTEGRITY | | | ALPOLIC | /PE | | | | | l and squared with |
| | | | TOTAL TH | ICKNESS | | edges to offer t | he best po | inel edge | e conditions in |
| | | | 3MM | 4MM | 6MM | the industry | | | |
| PROPERTY | UNIT | ASTM | .118" | 157" | .236" | | | | |
| Vertical Pull | psi | C-297 | 1906 | 1806 | 1664 | FIRE PERFOR | MANCE | | |
| Drum Peel | in-lb/in | D-1781 | 33.6 | 33.6 | 33.6 | | | | olyethylene core ho |
| Flatwise Shear | psi | C-273 | 1259 | 1225 | 1195 | | | | g laboratories usir |
| | | | | | | the following n | ationally r | ecognizi | ed fire tests. |
| ENGINEERING PROPE | RTIES | | ALPOLIC | /PE | | ASTM E84 | | | |
| | | | TOTAL TH | | | Flame spread: | - | mm | 0.5 |
| | | | 3MM | 4MM | 6MM | | | mm | 00 |
| PROPERTY | UNIT | ASTM | .118" | .157" | .236" | | - | mm | 00 |
| Aluminum Thickness | in | | .020 | .020 | .020 | Smoke develop | | mm | |
| Specific Gravity | | | 1.52 | 1.38 | 1.23 | | | mm | 00 |
| Weight | lbs/ff ² | | 0.93 | 1.12 | 1.50 | | 0 | mm | 10 |
| Coefficient of Expansion | in/in/ºF | D-696 | 13x10 ⁻⁶ | 13x10-6 | 13x10 ⁻⁶ | | | | |
| Thermal Conductance | BTU/hr/ºF/ff² | | 12.29 | 10.75 | 8.53 | ASTM E108 | MODIFIE | D | |
| Tensile Yield Strength | psi | E-8 | 8321 | 6429 | 4466 | | | mm | passed |
| Tensile Strength | psi | E-8 | 8747 | 6913 | 4978 | | | mm | passed |
| Elongation | % | E-8 | 12.1 | 13.5 | 17.3 | ASTM D192 | | | |
| Flexural Elasticity | psi | C-393 | 7110x10 ² | 5770x10 ² | 4220x10 ³ | Flash: | | mm | 716°F |
| Flexural Stiffness | psi | C-393 | 1.04x10 ^o | 1.99x10° | 4.98x10° | Ignition: | 4 | mm | 752°F |
| Punching Shear Resistance | | | | | | ASTM D635 | | | |
| Maximum Load | lbs | D-732 | 1847 | 1920 | 2121 | Rate of burning | 3: 4 | mm | Classified CC1 |
| Shear Resistance | psi | D-732 | 4950 | 4025 | 2816 | ASTM E162 | | | |
| Deflection Temperature | ۰F | D-648 | 231.8 | 231.8 | 231.8 | Flame spread: | 4 | mm | 0 |
| Sound Transmission Coefficient | STC# | E-90 | 25 | 26 | 26 | UL-879 | | | listed |
| | | | | | | UL-94 | | mm | V-O rating |
| | | | | | | CODE Evalu | ation Re | ports* | |
| SURFACE TREATMENT | 5 | | | | | 1. ICC ES | | | |
| a. 1.1.1.1.000.00 ² /00 | | | | <pre></pre> | | 2. City of Los | | | |
| Standard ALPOLIC [®] /PE w (LUMIFLON [™]) with a wid | | | | | | 3. Miami Da | | | |
| to meet AAMA 2605, pol | | | | | | 4. Floridga B | | ode Ap | proval |
| include Stone and Timber | | | | | | 5. UL Approv | red | | |
| | | | | | | * Reports are a | railable at | | |
| | | | | | | www.alpolic- | | | uments |
| STANDARD PANEL SI | ZES | | | | | | | | |
| | 146" | | | | | | | | |
| | 196" | | | | | | | | |
| 50" x 196" 62" > | | | | | | | | | |

Width 32.5"-62" (826mm - 1575mm) Length 6'-24' 2" (1829mm - 7315mm)



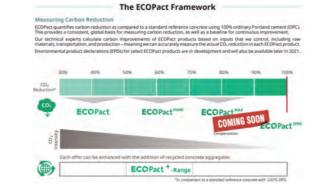




A Marriage of Energy Savings and Design Freedom



Kannen Company, Inc. 205 Gadheidge Gaart 276.449 3005 Technolog Pack/Alfans Roccess, GA.20072 kannener.com Charace Corpus, Inc. 201, 201 Perc Narder 17, 2024 7007 (Author 17, 2024) 7





KAWNEER



HCLEDECK





| | 11114 | AL BOTTOM AVERAGE BETWEEN SECTION UNLARGE OF C.S. INCREME AT REA WOLLY HE WIDTH THE RESS AREA | | | BETWEEN | - | 081880 | | | ILCODE GM | HADDINE (| - | | - | CONCRET |
|----------|--------|--|----------|--------------|---------|---------------|--------|---------------|---------|--------------|-----------|--------|---------|----------|---------|
| SPPINS . | NUMBER | | FROM TOP | ENDM BADE | 1000 | NUMBER TO THE | | WEIGHT VOLUME | | | | | | | |
| - | - | - | - | - | - 100 | | | 110409 | | | | 10,002 | 1000 | -1000 | |
| 50 | 100 | - | 245 | 800 | 4513 | 178 | 302 | 291317 | 16906.1 | 9047.1 | | | 648 | 0.296 | |
| 15 | 585 | 150 | 246 | 800 | 8719 | 181 | 284 | 376796 | 90094,9 | eMa.5 | 0.94 | 0,27 | -6.36 | 0,81 | |
| - 1001 | 560 | | .853 | 400 | 1913 | 180 | -962 | 443680 | 15466.6 | 8047,4 | | | 4.9 | 0,276 | |
| 50 | 500 | | .290 | ésó. | 1768 | 348 | 812 | 375629 | 15496,0 | 9007,1 | | - | 6.61 | 0,8% | |
| P5 | 525 | 200 | 296 | #50 | 1875 | 191 | 394 | 425242 | 15252.5 | 8722.1 | 0.18 | 0.24 | 7.08 | 0.281 | |
| 100- | 560 | | -300 | 450 | 2100 | 187 | 353 | 532394 | 14787,7 | 8252.6 | 1 | | 7,60 | 0.308 | |
| de. | . 0 | . 46 | - | | | | | | 100 | - | | × | 25 1240 | Concerte | |

| THERMAFIBER* RAINBARRIER* CI | Physica | al Properties | | | | | | | | | |
|--|---|-------------------------------------|-----------|-----------------------------------|----------------|-----------|-------------------------|-----------|-------|------------|----------|
| | PROPE | RTY | _ | TEST | METHO | _ | | | | | |
| GH COMPRESSIVE | Compre | ssive Strength | | ASTN | 1 C165 | | 5 kPa (720 0% deform | |) | | |
| PLUS (110) | Surface | | | CAN/ | ULC-S10 | Flar | ne Spread | i 0, Sm | oke | Develop | ed 5 |
| | Charact | eristics | | ASTN | 1 E84 | Flar | ne Spread | i 0, Sm | oke | Develop | ed O |
| IERAL WOUL INSULATION | Nes Ce | mbustibility | | CAN/ | ULC-S11 | Nor | Combust | tble | | | |
| | NOIPCO | noosionity | | ASTN | 1 E136 | Non | -Combust | ible as | defir | ned per N | IFPA 220 |
| | Smould | er Resistance | | CAN/ | ULC-S12 | Mea | in Mass L | oss < 0 | 0.02 | 5 | |
| | Linear S | hrinkage | | ASTN | 1 C356 | <2% | @ 650 °C | (1200 | ⊃°F) | | |
| | Water V | apour Permear | 00 | ASTN | 1 E96 | 2,63 | 1 ng/Pa•s | ;•m² (4 | l6 Pe | erms) | |
| | Water V | apour Sorption | | ASTN | 1 C1104 | <0.5 | 3% | | | | |
| escription | | Fungi Resistance | | | 1 C1338 | Pas | s | | | | |
| tinuous insulation boards are designed | Corrosion of Steel, Aluminum, and Copper | | | ASTN | 1 C665 | Pas | s | | | | |
| superior compressive strength while | | Stress Corrosion – Austenitic Steel | | ASTM C795 | | Pass | | | | | |
| GH COMPRESSIVE PLUS (110) IERAL WOOL INSULATION | Odor | | | ASTM C1304 Pass | | | | | | | |
| | Techni | cal Data | | | | | | | | | |
| | | TO ASTM CS | 18 | | | TES | TED TO C | AN/UI | LC-S | 3102 UN | FACED |
| t system with minimal penetration ntinuous insulation | RSI /25. 24 °C m | 4 mm (i) F-K/W | R-v 75 | alue/in: °F.hr-ft ¹ | ch @ WF/Btu | Flarr | e Spread | | Sm | oke Devi | sloped |
| tible and non-deteriorating ve energy/reduce greenhouse gas | 0.73 | | 4.1 | | | 0 | | | 5 | | |
| acoustical performance 10% recycled content? | Acoust | ical Perforn | an | ce | | | | | | | |
| to credits in several green building uch as LEED [®] and Green Globes [®] | | THICKNESS | | 125 HZ | 250 HZ | 500 HZ | 1000 HZ | 200 HZ | • | 4000 HZ | NRC |
| | ASTM | 32 mm (1.25 | 5 | 0.11 | 0.52 | 0.99 | 1.01 | 1.01 | | 1.00 | 0.90 |
| ode Compliance ation Listing No. 14060-L | C423 | 51 mm (2*) | | 0.27 | 0.89 | 0.95 | 1.04 | 1.00 | | 1.00 | 0.95 |
| 5702, Standard for Mineral Fibre Thermal | | 102 mm (4*) | 1 | 0.57 | 0.79 | 0.95 | 0.99 | 0.99 | | 0.99 | 0.95 |





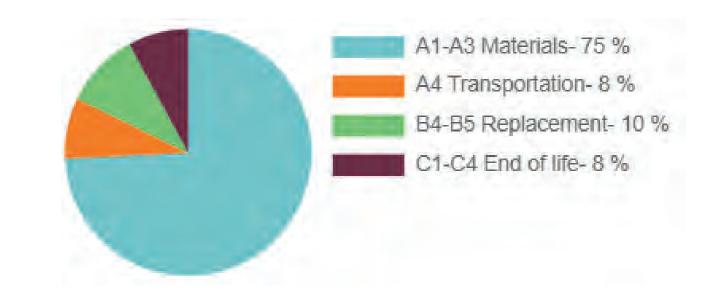
INVENTORY BY FLOOR

EMBODIED CARBON AND CLASSIFICATIONS

| | COUNT | M2 | M3 |
|------------------------------------|-------|------|--------|
| Doors | 92 | | |
| Door | 74 | | |
| Main Door | 18 | | |
| Aluminum 6061 | | | |
| Single emergency door | 6 | | |
| Double emergency door | 1 | | |
| Cast-in-place concrete | | | 166.27 |
| Concrete slab topping | | 1050 | 36.75 |
| Damp-proofing floor | | 1050 | |
| Gypsum Wall Board interior | | 5111 | 96.55 |
| Light gauge steel framing, thermal | | | |
| air layer | | 1923 | |
| Light gauge steel furring | | 1504 | |
| physical material (floor) | | 1050 | 472.5 |
| Polyethylene film membrane | | 1504 | |
| Precast concrete (substitute with | | | |
| Comfloor) | | 1050 | 237.3 |
| Rigid foam insulation board | | 1564 | 105.98 |
| Soda Lime Glass | | 391 | |
| Steel 345 Mpa (Alum, Composite) | | 602 | |
| Vinyl Composition Tile | | 1050 | |
| Wood framing, insulated /st. studs | | 1281 | 126.68 |
| LED | 75 | | |
| Ductwork (to be adjusted) in kg | 2575 | | |

Embodied carbon by structure - A1-A3 Foundations and substructure - 1% Vertical structures and facade - 49% Horizontal structures: beams, floors and roofs - 25% Other structures and materials - 24% 20% 40% 60% 0%

Embodied carbon by life-cycle stage



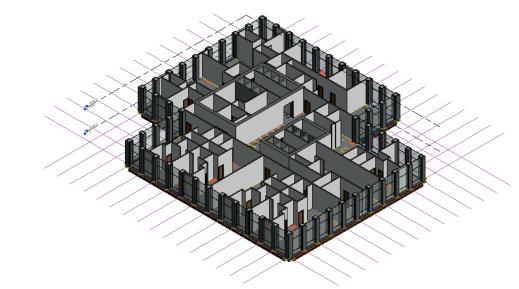
Global warming kg CO2e - Classifications

- Floor slabs, ceilings, roofing decks, beams and roof 25.7% Columns and load-bearing vertical structures 16.7% Total water consumption 15.9%

- Finishes and coverings 13.0% Internal walls and non-bearing structures 10.5%
- External walls and facade 7.6%
- Electricity use 5.5%
- Windows and doors 2.3%
- Other structures and materials 2.0%
- Foundation, sub-surface, basement and retaining walls 0.7%

Global warming kg CO2e - Resource types

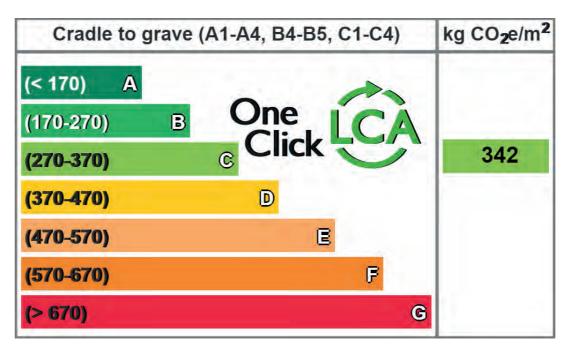




ONE CLICK LCA RESULT

MOST CONTRIBUTING MATERIALS (GLOBAL WARMING)

| No. | Resource | Cradle to gate impacts (A1-A3) | Of cradle to gate (A1-A3) | Sustainable alternatives |
|-----|--|--------------------------------|---------------------------|-------------------------------|
| 1. | Ready-mix concrete, high-strength, generic 🚥 ? | 99 tons CO ₂ e | 37.0 % | Show sustainable alternatives |
| 2. | Aluminum composite panel, curtain walling/facade, mineral filled ? | 43 tons CO ₂ e | 16.2 % | Show sustainable alternatives |
| 3. | Triple pane insulated glass unit (IGU) with two spacer 🔤 ? | 33 tons CO ₂ e | 12.4 % | Show sustainable alternatives |
| 4. | Galvanized steel profiles, furrings (F-section) 🐵 ? | 28 tons CO2e | 10.6 % | Show sustainable alternatives |
| 5. | Gypsum plaster board, regular, generic 🔤 ? | 15 tons CO ₂ e | 5.6 % | Show sustainable alternatives |
| 6. | Reinforcement steel (rebar), generic 💩 ? | 15 tons CO2e | 5.5 % | Show sustainable alternatives |
| 7. | Luxury vinyl floor tile 🚥 ? | 11 tons CO ₂ e | 4.0 % | Show sustainable alternatives |
| 8. | Glass wool acoustic ceiling panel 🚳 ? | 6.2 tons CO ₂ e | 2.3 % | Show sustainable alternatives |
| 9. | Wooden door, with wooden frame ? | 4.5 tons CO ₂ e | 1.7 % | Show sustainable alternatives |
| 10. | Pre-insulated round ductwork system for HVAC ? | 4 tons CO ₂ e | 1.5 % | Show sustainable alternatives |
| 11. | LED office lighting 🐵 ? | 2.5 tons CO2e | 0.9 % | Show sustainable alternatives |
| 12. | Ready-mix concrete, normal-strength, generic 🚳 ? | 1.7 tons CO ₂ e | 0.6 % | Show sustainable alternatives |
| 13. | Glass wool insulation panels, unfaced, generic 🐵 ? | 1.4 tons CO ₂ e | 0.5 % | Show sustainable alternatives |
| 14. | Steel door with polystyrene core, per unit ? | 1.1 tons CO ₂ e | 0.4 % | Show sustainable alternatives |
| 15. | Diffuser, HVAC, French average 🔤 ? | 0.91 tons CO ₂ e | 0.3 % | Show sustainable alternatives |
| 16. | Reinforcement steel (rebar), generic 🔤 ? | 0.59 tons CO2e | 0.2 % | Show sustainable alternatives |
| 17. | Damp insulation PA 💩 ? | 0.25 tons CO2e | 0.1 % | Show sustainable alternatives |
| 18. | Deep foundation concrete piles ? | kg CO ₂ e | 0.0 % | Show sustainable alternatives |
| 17. | Emergency exit light 🚳 ? | 26 kg CO ₂ e | 0.0 % | Show sustainable alternatives |
| 18. | Etherðeuch exir líður 🔜 🚦 | 20 ng 0020 | 0.0 /0 | onow oustainable alternatives |



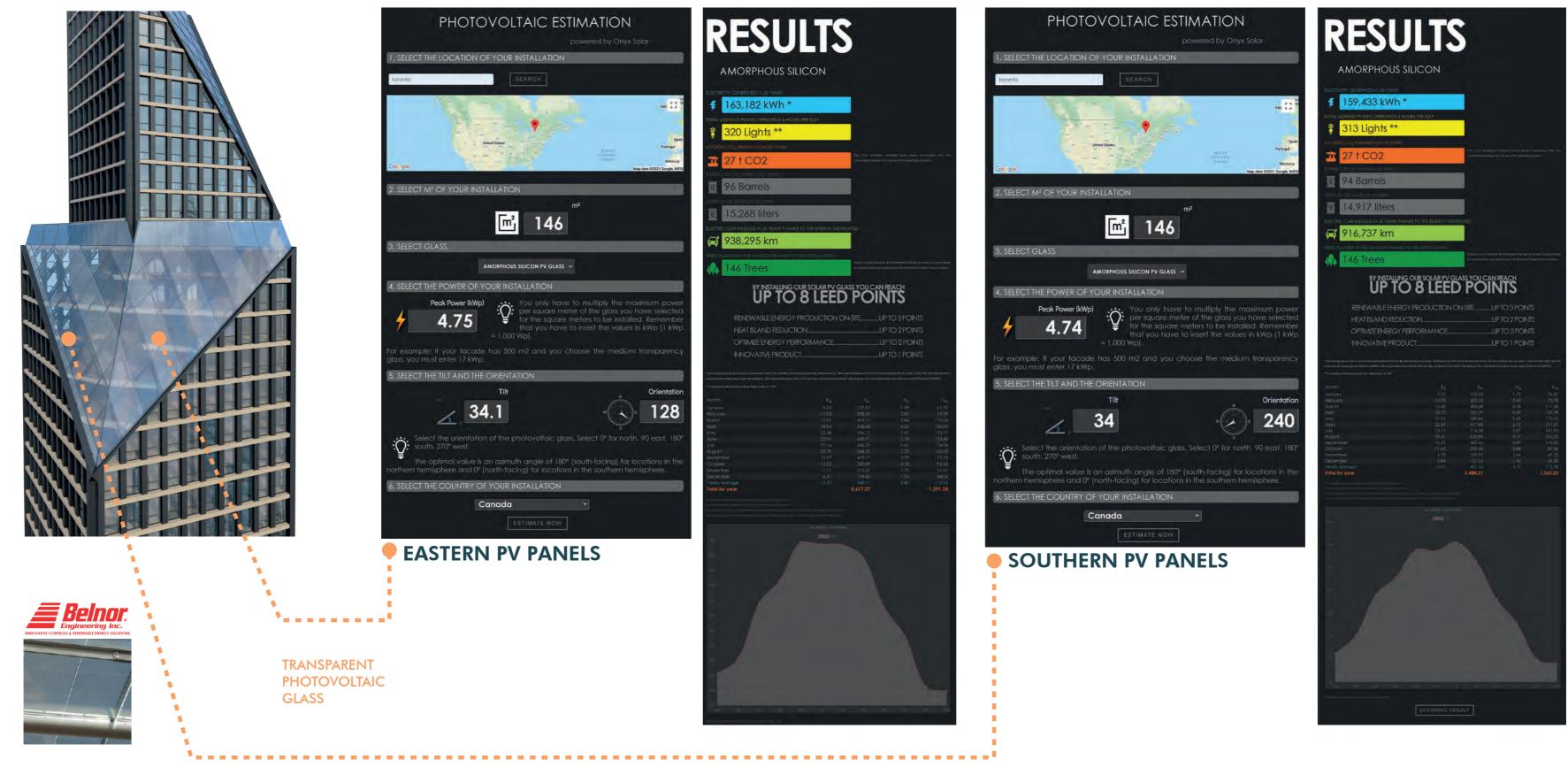
8.32 kg CO2e / m2 / year

327 kg CO2e / m2

Further efficiency could be achieved with three strategies: volume Lessen the total |. and metals. concrete ot 2. Replacement of certain products with more energy-efficient ones (e.g., acoustic ceiling panels). 3. Use of energy/water-efficient appliances to reduce total usage.

| POLITECNICO MILANO 1863 | MSC BUILDING ARCHITECTURE THESIS | PROFESSORS: MARIA GRAZIA FOLLI CORRADO PECORA GIOVANNI DOTELLI FRANCESCO ROMANO MARCO IMPERADORI | STUDENTS: JUAN CARLOS MEDINA MARIA JOSE MONTERO DIANA MARISOL NARVAEZ | 10702592 10712731 10704376 | OUR BEACON: TORONTO AFFORDABLE HOUSING | 11 26 |
|-----------------------------------|-------------------------------------|---|--|----------------------------------|--|----------|
|-----------------------------------|-------------------------------------|---|--|----------------------------------|--|----------|

PV PANEL POTENTIAL ACCORDING TO MANUFACTURER'S PARTNER



CONSTRUCTIVE DETAILS SLAB DETAILS

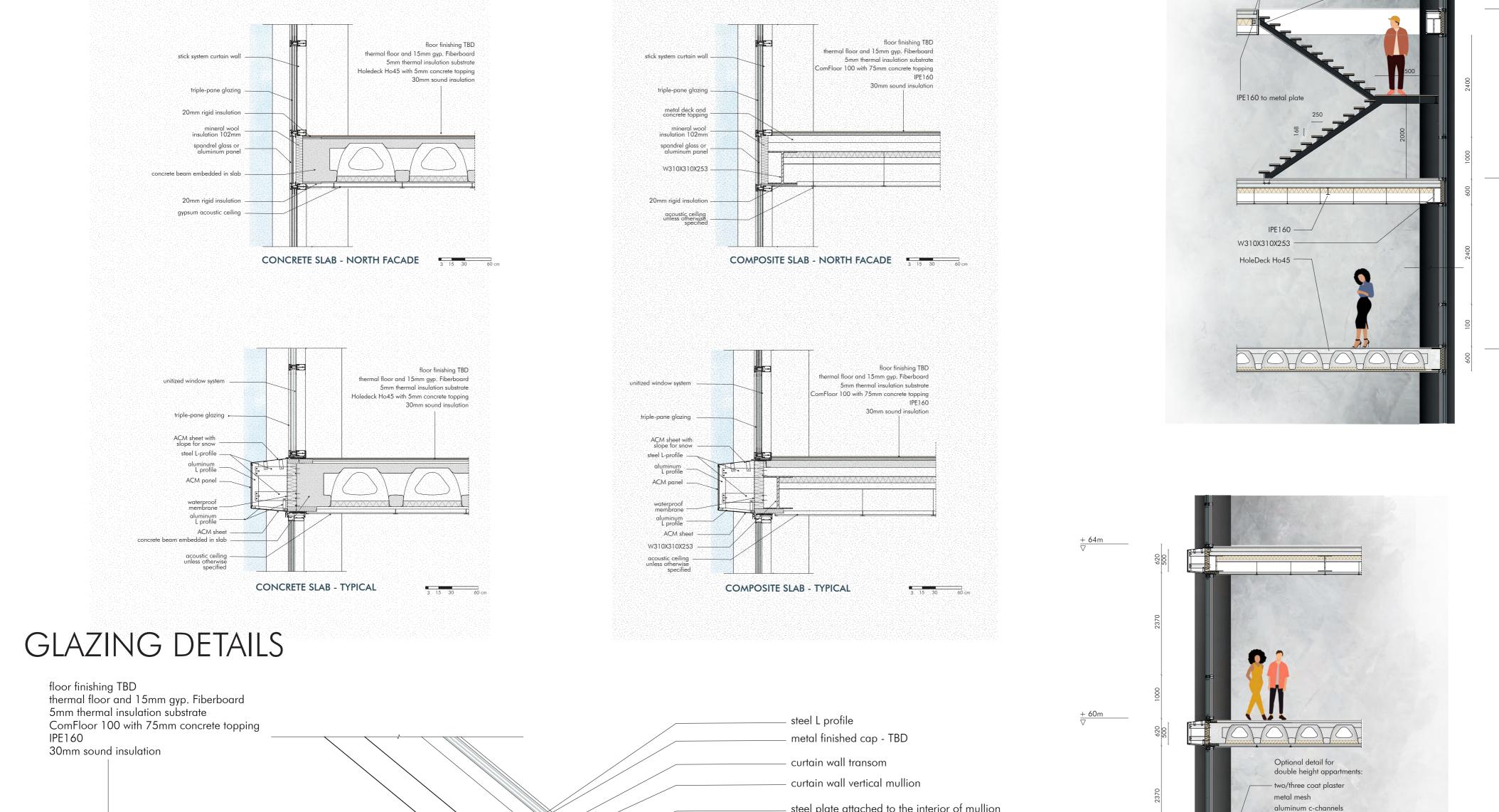


L profiles

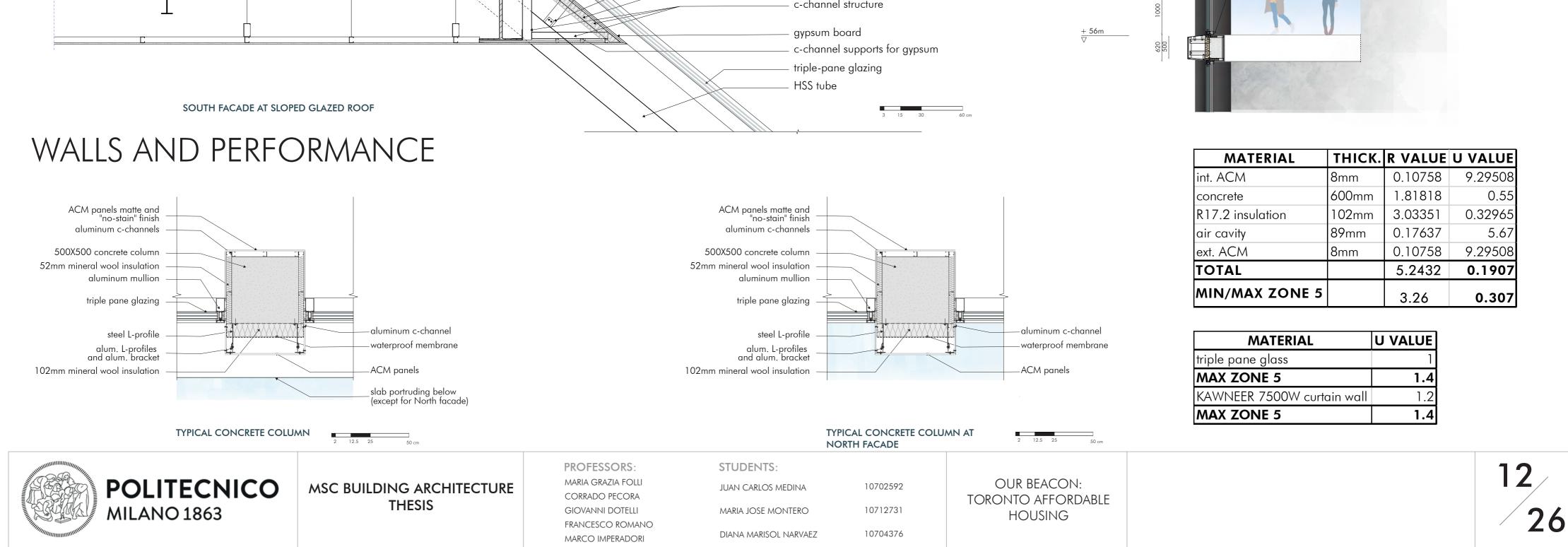
attached to beam

+ 64m

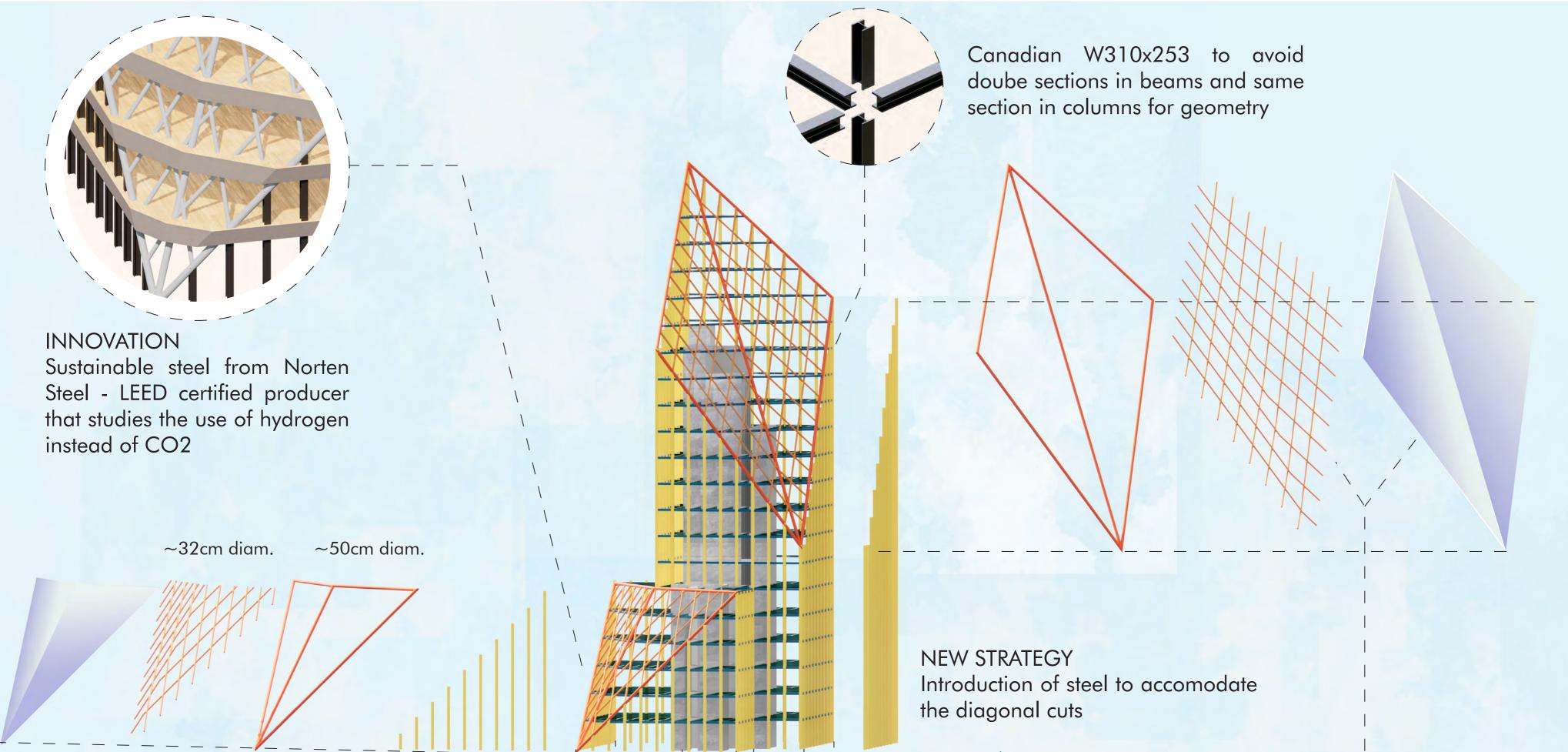
+ 60m



steel plate attached to the interior of mullion anchor welded to tube mineral wool insulation

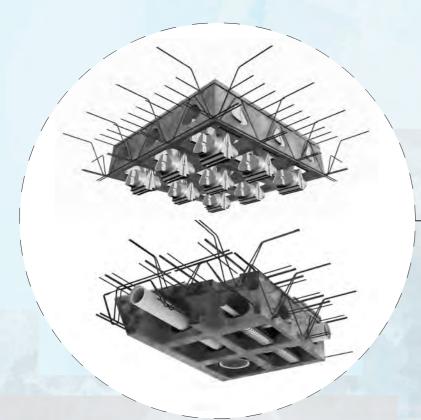


STRUCTURE



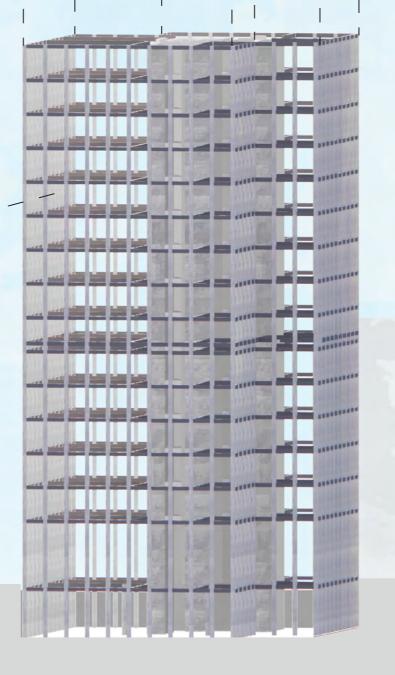


INNOVATION



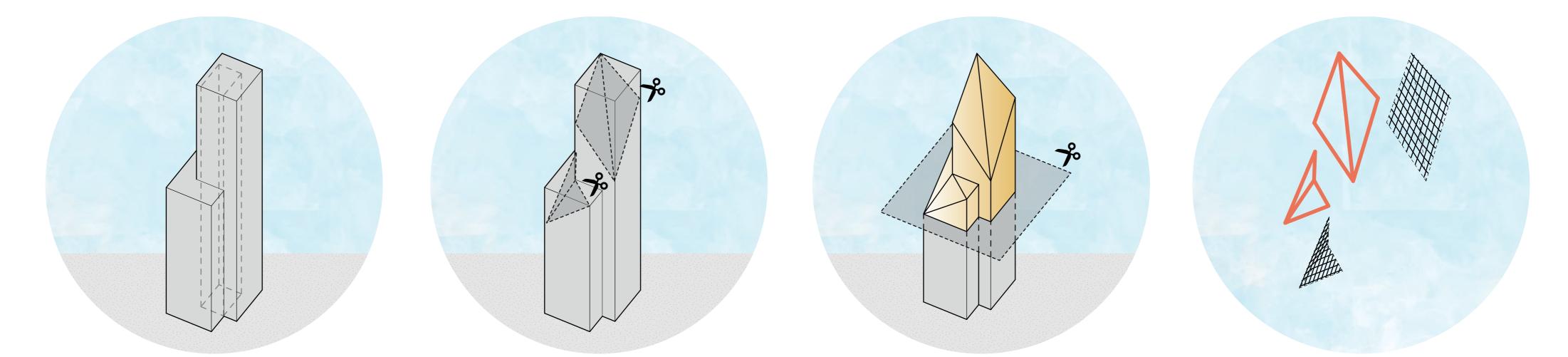
INNOVATION Holedeck Ho45 allows for maximum span with a shallower slab and less concrete

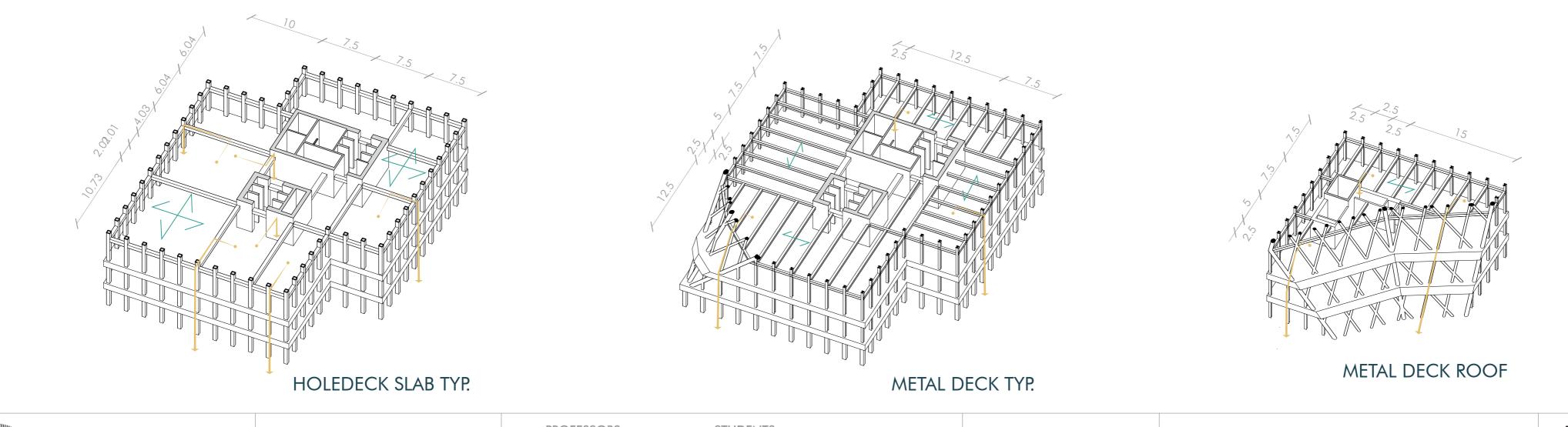
STRUCTURAL CONCEPT



Orthogonal grid for the diamonds allows for easier installation of triple pane glazing for better thermal performance

TRADITIONAL STRATEGY Concrete column , beam and core construction







MSC BUILDING ARCHITECTURE THESIS

PROFESSORS: MARIA GRAZIA FOLLI CORRADO PECORA GIOVANNI DOTELLI FRANCESCO ROMANO MARCO IMPERADORI

STUDENTS: JUAN CARLOS MEDINA MARIA JOSE MONTERO DIANA MARISOL NARVAEZ

10702592

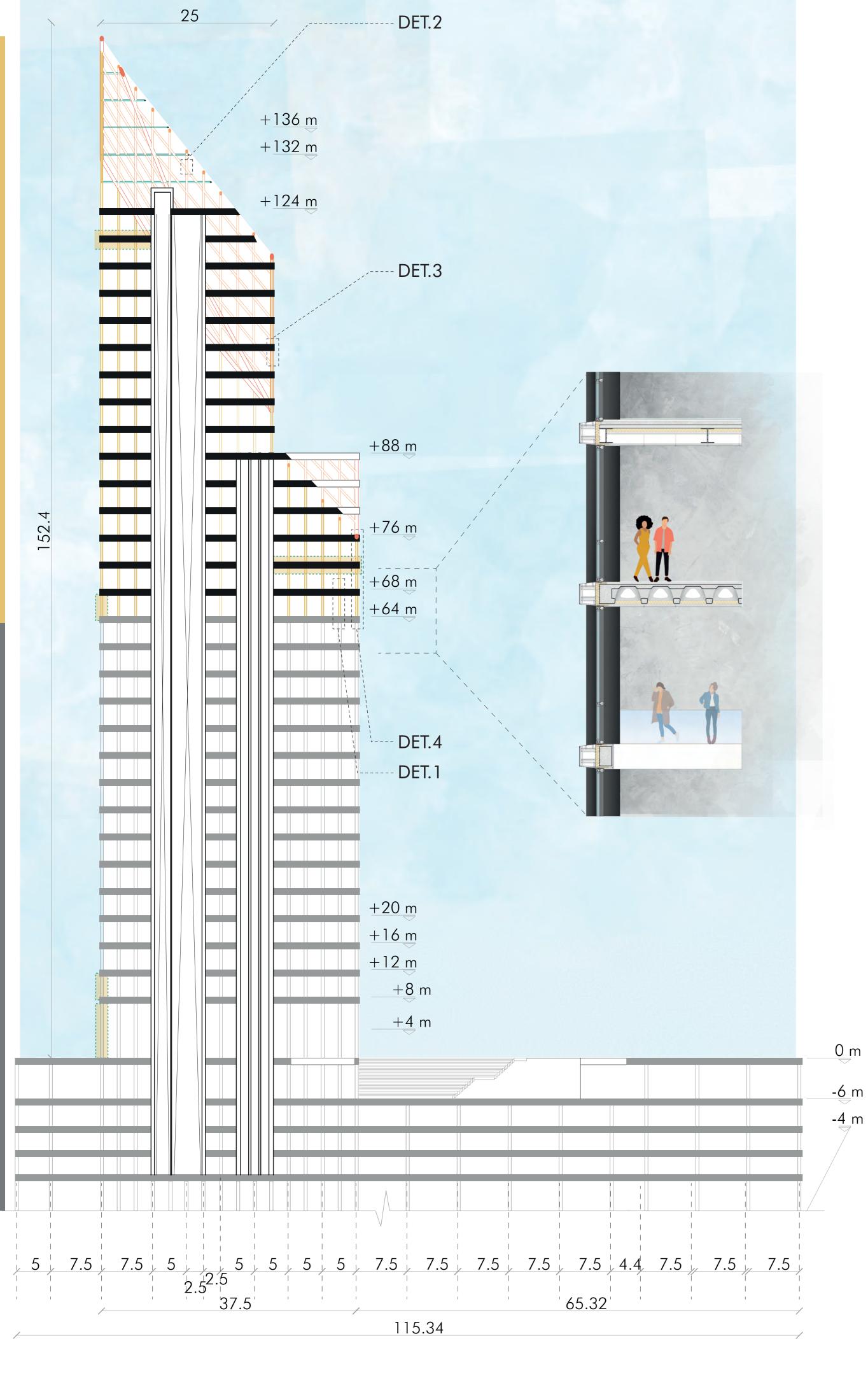
10712731

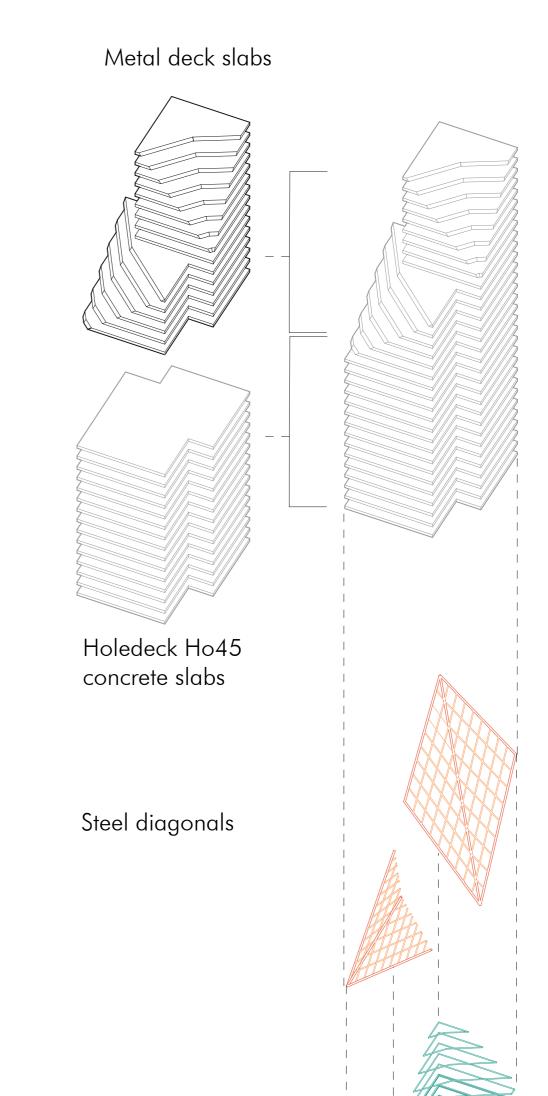
10704376

OUR BEACON: TORONTO AFFORDABLE HOUSING



STRUCTURAL SECTION



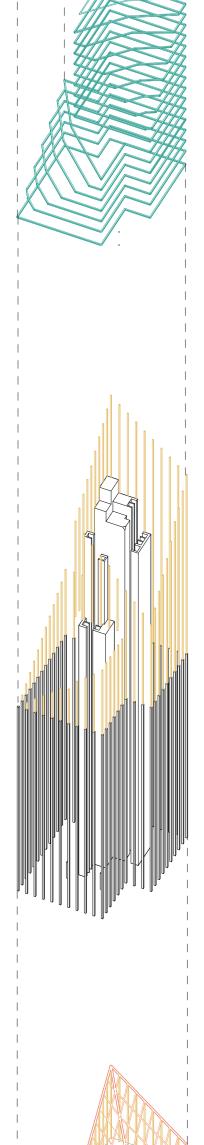


STEEL

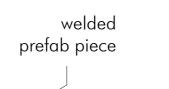


Steel horizontal bracing at steel deck levels

Concrete core and concrete columns plus steel columns above 64m.



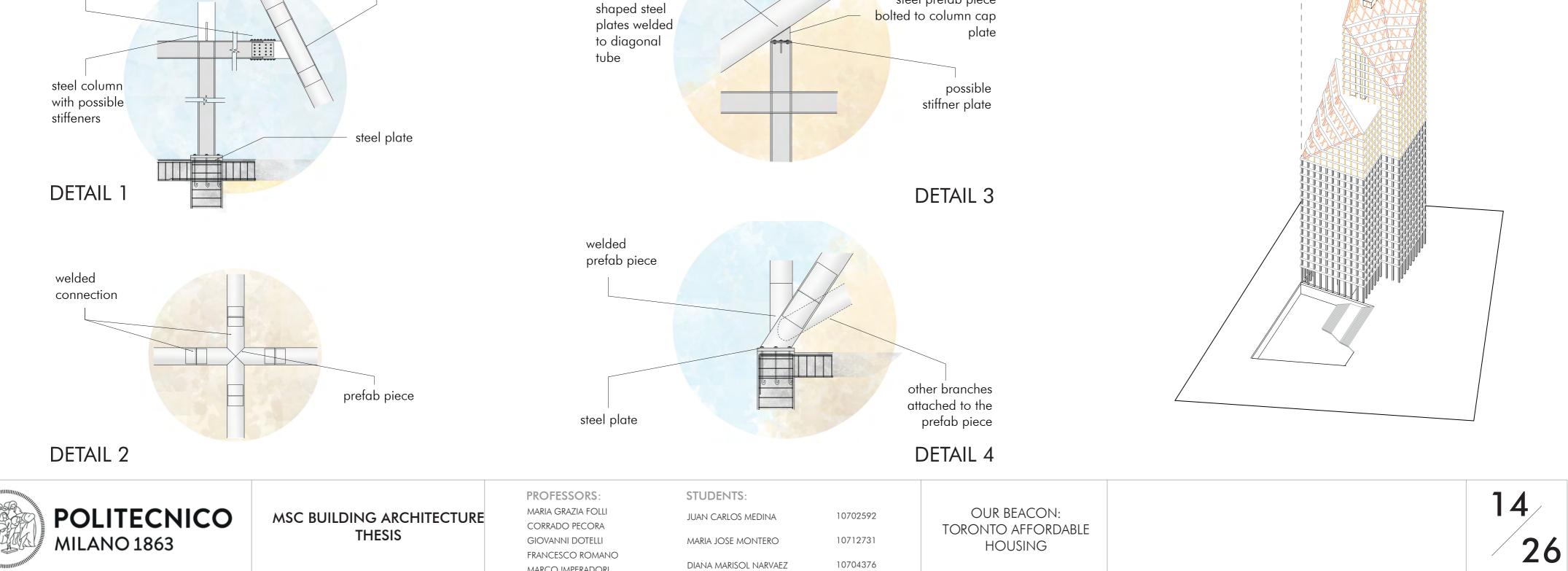
bolted joint with top and bottom plates



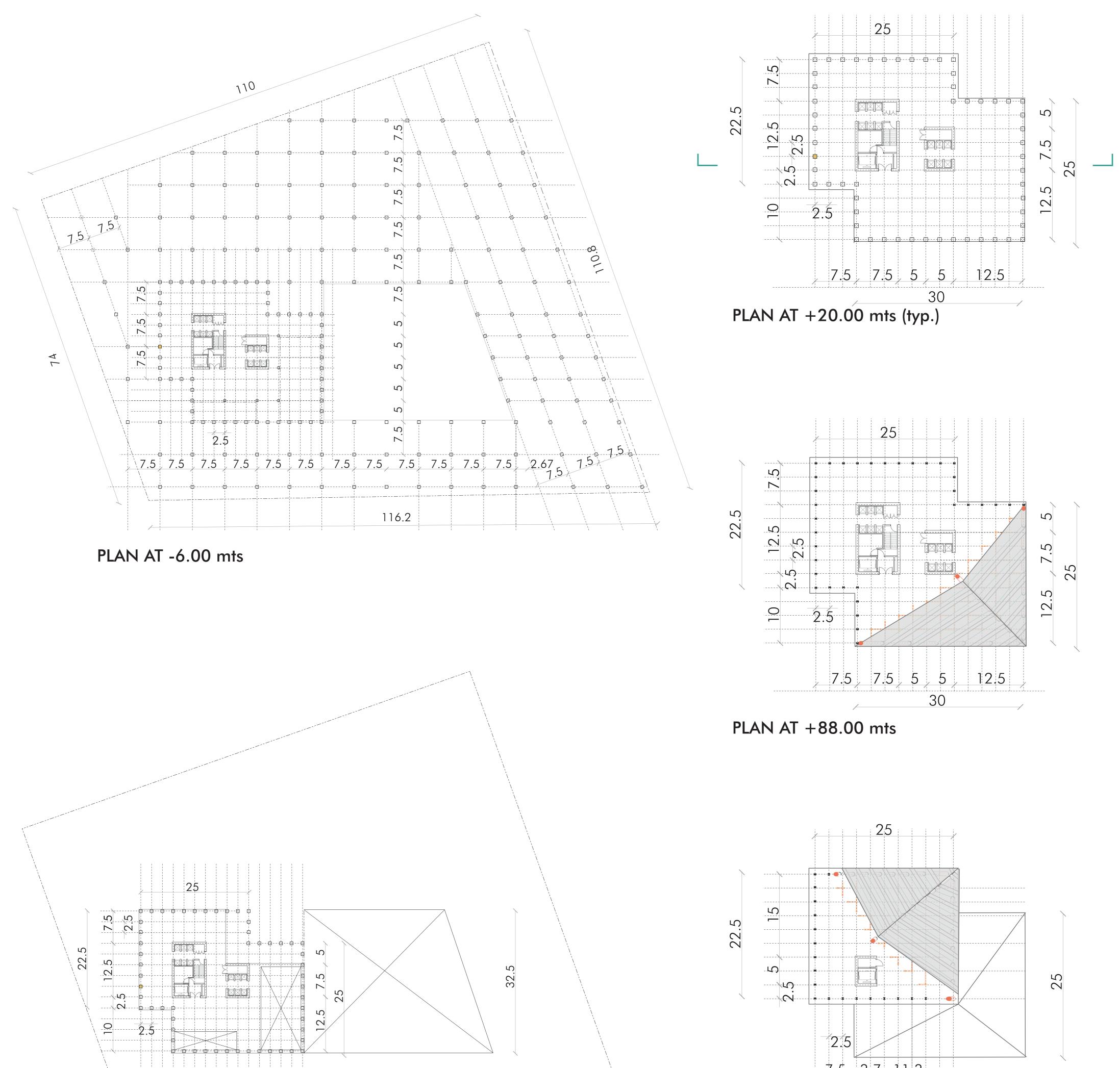
two or more steel prefab piece

custom

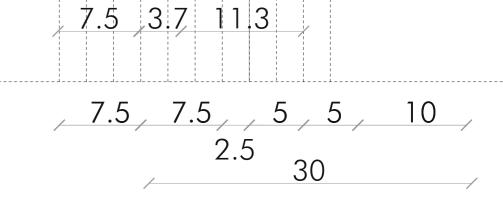
MARCO IMPERADORI



TYPICAL PLANS







PLAN AT 0.00 mts

PLAN AT +124.00 mts

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|-----------------------------------|-------------------------------------|---|--|----------------------------------|--|----------|
| - ANNI MARKE | | MARCO IMPERADORI | DIANA MARISOL NARVAEZ | 10/043/0 | | |

RESULTS

| | MATERIAL | DENSITY | THICKNESS | WEIGHT |
|---|-----------------------------------|-------------|-----------|---------------|
| | | - | - | |
| | floor finishing | | 10mm | 11.24 daN/m2 |
| | thermal floor and gyp. Fibreboard | | 15mm | 40.00 daN/m2 |
| | thermal insulation substrate | | 5mm | 2.00 daN/m2 |
| ~ | concrete (total 150mm deck) | 2400 daN/m3 | 100mm | 240.00 daN/m2 |
| G | metal deck (ComFlor 100) | | 100mm | 8.16 daN/m2 |
| | insulation | | 30mm | 10.00 daN/m2 |
| | acoustic ceiling | | 25mm | 18.00 daN/m2 |
| | services | | | 50.00 daN/m2 |
| | | | | 379.40 daN/m2 |
| | | | | 3.72 kN/m2 |

| 0 | ROOF: CATEGORY | WEIGHT | | | | |
|---|-----------------|------------|--|--|--|--|
| Q | Public Terraces | 5.00 kN/m2 | | | | |

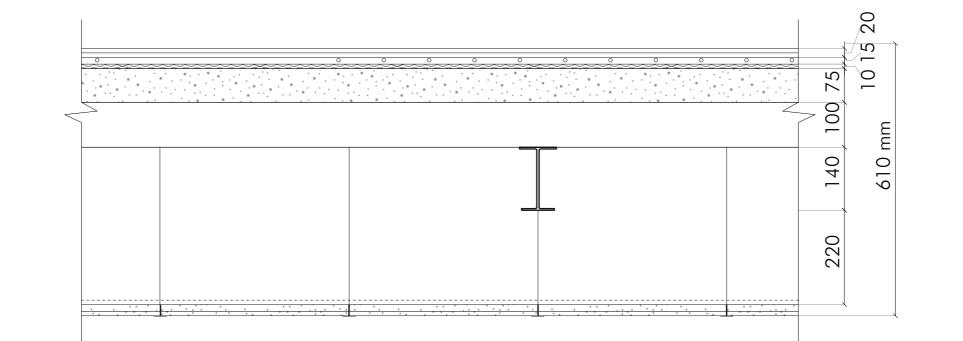
| | FLOOR: CATEGORY | WEIGHT | ٦ |
|---|---|-----------|---|
| G | Areas with possible physical activities | 5.00 kN/m | 2 |

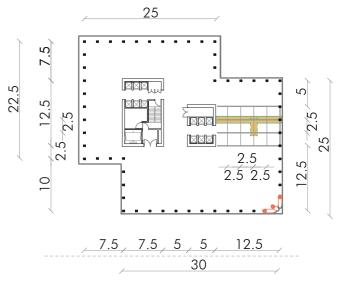
STEEL DECK SLAB SECTION

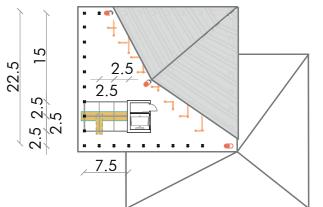
| | MATERIAL | DENSITY | THICKNESS | WEIGHT |
|---|-----------------------------------|---------|-----------|---------------|
| | | · | · | • |
| | floor finishing and grout | | 20mm | 11.24 daN/m2 |
| | thermal floor and gyp. Fibreboard | | 15mm | 40.00 daN/m2 |
| | thermal insulation substrate | | 5mm | 2.00 daN/m2 |
| G | holedeck Ho45 and 50mm topping | | 500mm | 565.00 daN/m2 |
| | sound insulation | | 30mm | 10.00 daN/m2 |
| | acoustic ceiling | | 25mm | 18.00 daN/m2 |
| | services | | | 50.00 daN/m2 |
| | | | | 696.24 daN/m2 |
| | | | | 6.96 kN/m2 |

| | CATEGORY | WEIGHT |
|---|---|------------|
| Q | Areas with possible physical activities | 5.00 kN/m2 |

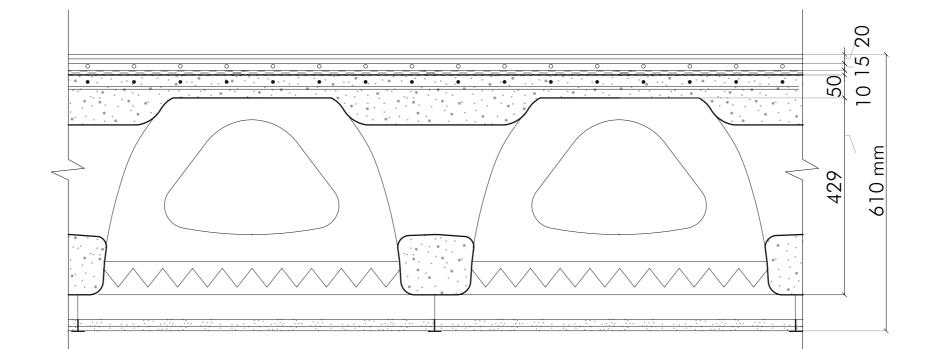
HOLEDECK Ho45 SLAB SECTION

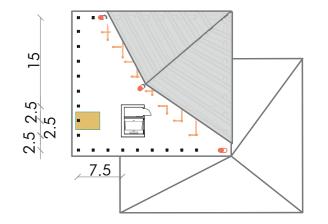






25





| | G+Q | |
|------------------|------|------------------|
| | | |
| \bigtriangleup | | \bigtriangleup |
| | 0.5 | I |
| R1 | 2.5m | R2 |

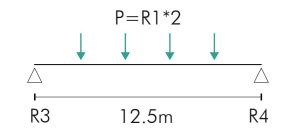
| | ULS | SLS |
|-----------|------------|------------|
| G | 4.84 kN/m2 | 3.72 kN/m2 |
| Q | 7.50 kN/m2 | 5.00 kN/m2 |
| BEAM | 0.60 kN/m | 0.78 kN/m |
| LINEAR W. | 31.62 kN/m | 22.40 kN/m |
| | | |

| | MAX/LIM. | REQUIRED | IPE 160 |
|----------|------------|-----------|------------|
| SHEAR | 39.52 kN | 1.17 cm2 | 9.66 cm2 |
| MOMENT | 24.70 kN m | 73.06 cm3 | 108.70 cm3 |
| D. TOTAL | 0.0100 m | | 0.0062 m |
| D. Q | 0.0083 m | | 0.0035 m |



 \wedge

spacing: 2.5m FLOOR: SECONDARY BEAM



spacing: 2.5m FLOOR: PRIMARY BEAM

| | ULS | SLS |
|---------------|-----------|-----------|
| P=R*2 | 79.05 kN | 56.00 kN |
| $Ptot = P^*4$ | 316.19 kN | 223.99 kN |
| R3=R4 | 158.09 kN | 112.00 kN |

MAX/LIM. REQUIRED W310x310x253 323 cm2 158.09 kN 4.68 cm2 SHEAR APPROVED **MOMENT** 592.85 kN m 1753.50 cm3 3833 cm3 **D. TOTAL** 0.0500 m 0.0481 m 0.0107 m 0.0417 m D. Q

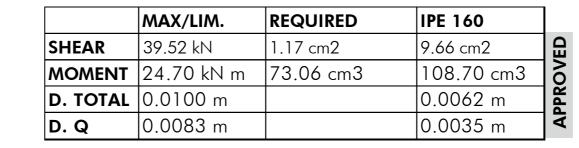






spacing: 2.5m ROOF: SECONDARY BEAM

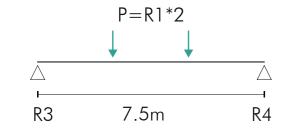
| | ULS | SLS |
|-----------|------------|------------|
| G | 4.84 kN/m2 | 3.72 kN/m2 |
| Q | 7.50 kN/m2 | 5.00 kN/m2 |
| BEAM | 0.60 kN/m | 0.78 kN/m |
| LINEAR W. | 31.62 kN/m | 22.40 kN/m |









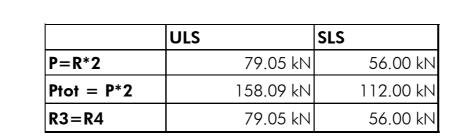


spacing: 2.5m ROOF: PRIMARY BEAM

700X700

D12 stirrups

14 rebars D32 and

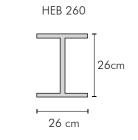




| | G | Q AVG |
|-------------|-------------|-------------|
| FLOORS (14) | 97.47 kN/m2 | 44.80 kN/m2 |
| FLOORS (16) | 59.51 kN/m2 | 56.50 kN/m2 |

| Ned | 3504.70 kN | |
|-----|--------------|--|
| ULS | 356.03 kN/m2 | |

| | MAX/LIM. | REQUIRED | HEB 260 | |
|----------|-------------|------------|-----------|--|
| SHEAR | 79.05 kN | 2.34 cm2 | 37.59 cm2 | |
| MOMENT | 197.62 kN m | 584.50 cm3 | 1148 cm3 | |
| D. TOTAL | 0.0300 m | | 0.0268 m | |
| D. Q | 0.0250 m | | 0.0036 m | |



| Δ | Δ | Δ |
|---|---|---|
| | | |

| CONCRETE | C80/95 |
|----------|---------------|
| fcd | 95000 kN/m2 |
| fyd | 500000 kN/m2 |
| E | 4224000 kN/m2 |

| | MAX/LIM. | 700X700 | |
|-------------|-----------|------------|-----|
| COMPRESSION | 1 | 0.1 | |
| BUCKLING | 3504.7 kN | 35856.8 kN | PRC |
| SLENDERNESS | 39.590 | 39.892 | ΔP |

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GR. FLOOR COLUMN

area: $2.5m \times 3.75m = 9.4m^2$

•

L = 8m

NED accounts for 5% weight increase for structure



area: $2.5 \text{m} \times 3.75 \text{m} = 9.4 \text{m}^2$ L = 4m1 st FLOOR COLUMN

| | G | Q AVG. |
|-------------|-------------|-------------|
| FLOORS (13) | 90.51 kN/m2 | 39.93 kN/m2 |
| FLOORS (16) | 59.51 kN/m2 | 56.50 kN/m2 |

ULS 339.68 kN/m2 NED 3343.68 kN

| CONCRETE | C50/60 |
|----------|----------------|
| fcd | 60000 kN/m2 |
| fyd | 500000 kN/m2 |
| E | 37278000 kN/m2 |

| | MAX/LIM. | 500X500 | |
|-------------|-----------|------------|--|
| COMPRESSION | 1 | 0.2 | |
| BUCKLING | 3343.7 kN | 12876.0 kN | |
| SLENDERNESS | 27.713 | 27.74 | |

NED accounts for 5% weight increase for structure

| 35.6cm | n W310X310 X253 |
|--|-------------------------|
| 31.9 cm | |
| area: 2.5m x 3 L = 4m 15th FLOOR C | 8.75m = 9.4m2 COLUMN |

| | G | | Q AVG. |
|-------------|---|-------------|-------------|
| FLOORS (15) | | 55.79 kN/m2 | 52.97 kN/m2 |

| ULS | 152.55 kN/m2 |
|-----|--------------|
| Ned | 1501.67 kN |

Section chosen for its geometry. NED accounts for 5% weight increase for structure

| STEEL | S355 |
|-------|----------------|
| Fy | 355000 kN/m2 |
| lz | 21460 cm4 |
| E | 21000000 kN/m2 |

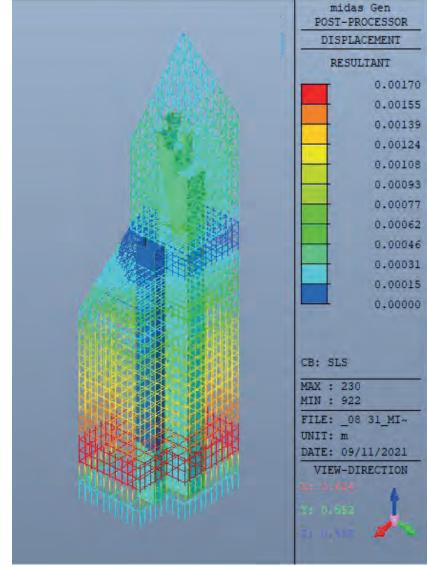
| | MAX/LIM. | W310x310x253 | /ED |
|-------------|-----------|--------------|-----|
| COMPRESSION | 1 | 0.1375 | Ő |
| BUCKLING | 1501.7 kN | 27799.0 kN | PPR |
| SLENDERNESS | 1501.669 | 11836.418 | A |

| POLITECNICO MILANO 1863 | MSC BUILDING ARCHITECTURE THESIS | PROFESSORS: MARIA GRAZIA FOLLI CORRADO PECORA GIOVANNI DOTELLI FRANCESCO ROMANO | STUDENTS: JUAN CARLOS MEDINA MARIA JOSE MONTERO DIANA MARISOL NARVAEZ | 10702592 10712731 10704376 | OUR BEACON: TORONTO AFFORDABLE HOUSING | 16 26 |
|-----------------------------------|-------------------------------------|---|--|----------------------------------|--|----------|
| | | MARCO IMPERADORI | DIANA MARISOL NARVAEZ | 10704376 | | |

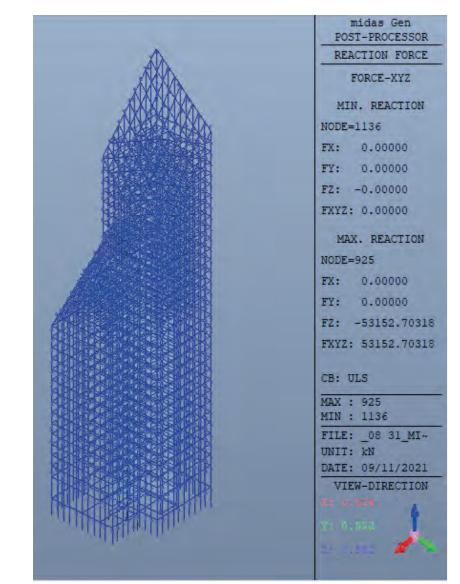
MIDAS ANALYSIS

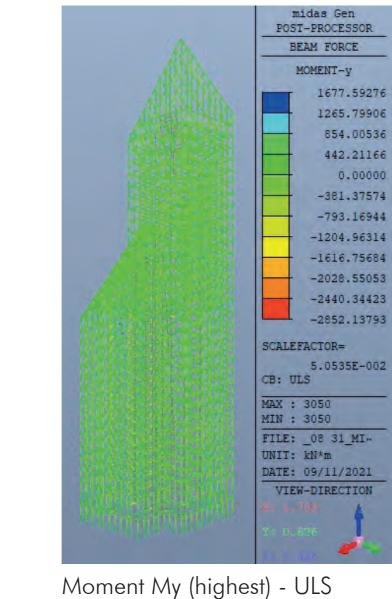
FULL BUILDING ANALYSIS

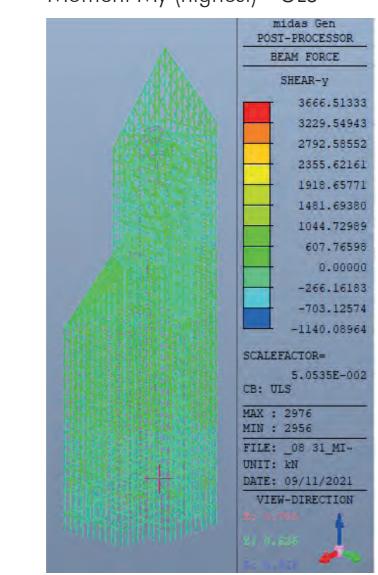
STEEL CODE CHECK



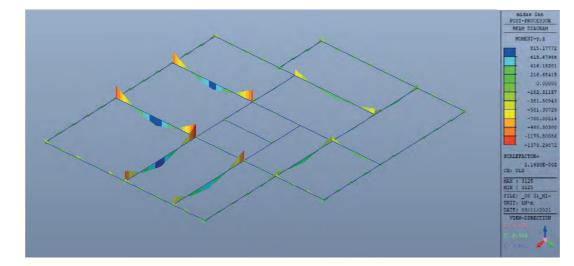
Deflection Analysis - SLS



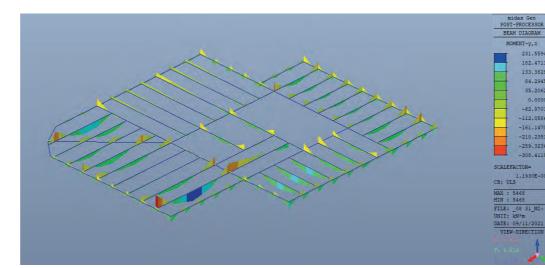




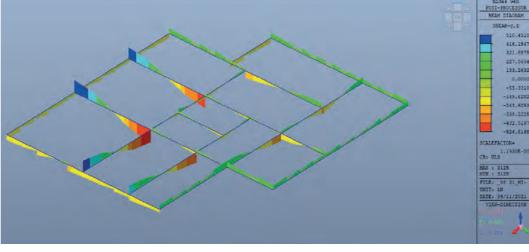
Shear Fy (highest) - ULS



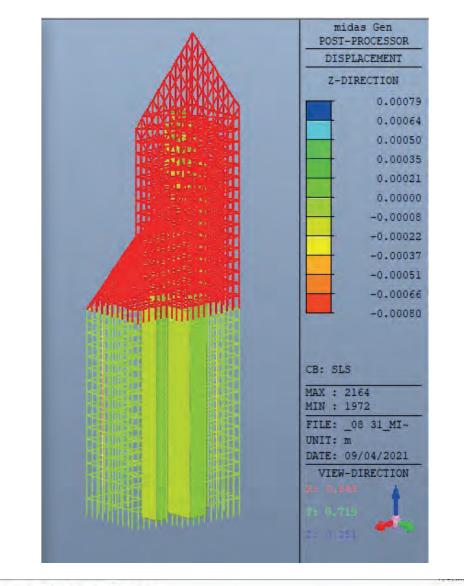
Concrete Floor Moment Mzy - ULS



Steel Floor Moment Mzy - ULS

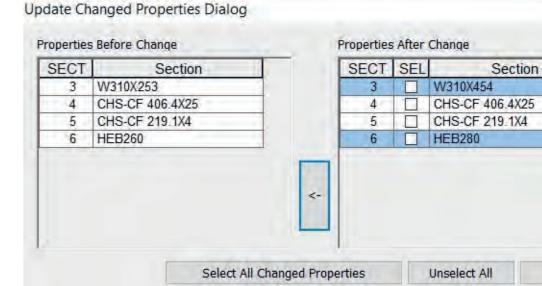


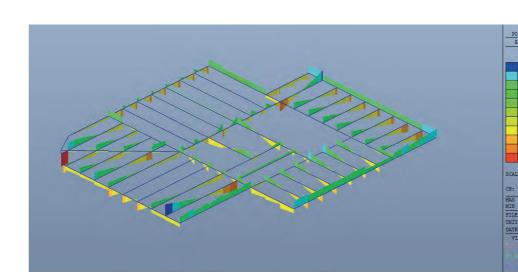
Concrete Floor Shear Fzy - ULS



X

Close





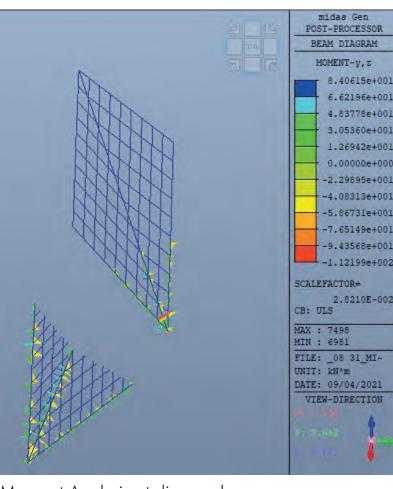
Steel Floor Shear Fzy - ULS

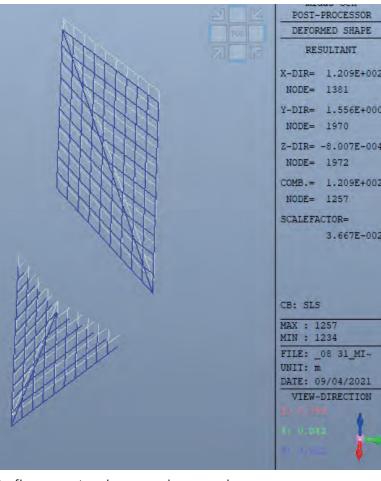
| | Euroco | de3:05 | | | Ur | nit: I | (N ;) | m | Prima | ry Sortin | ng Option | 1 | | | | | | |
|-------|--------|--------|-----|-----------|--------|--------|---------------|--------|-------|-----------|-----------|--|--------|--------|--------|--------|--------|--------|
| orted | bγ | O Men | | Ch | ange | | Update | | ି ଶ | ECT | ME | MB | | | | | | |
| CH | MEM | SEC | SE | Sectio | n | LC | Len | Ly | Ky | Bmy | N,Ed | My,Ed | My,Ed | Mz,E | Vy,Ed | Vz,Ed | T,Ed | Def |
| K | COM | SHR | L | Material | Fy | В | Lb | Lz | Kz | Bmz | N,Rd | Mb,R | My,R | Mz,R | Vy,Rd | Vz,Rd | T,Rd | Defa |
| ok - | 5675 | 3 | E | W310X4 | 54 | 4 | 0.8419 | 0.8419 | 1.000 | 0.881 | 380.95 | 19.006 | 19.006 | -96.81 | -83.89 | 20.444 | - | -0.003 |
| UN | 0.098 | 0.009 | 100 | S355 | 33500 | a | 2.5000 | 0.8419 | 1.000 | 0.847 | 19329. | 0.0000 | 2948.0 | 1340.0 | 8946.6 | 3194.4 | - ÷ | 0.050 |
| ok - | 7504 | 4 | F | CHS-CF 40 | 5.4X25 | 4 | 0.4778 | 0.4778 | 1.000 | 0.913 | 46.132 | 94.698 | 94.698 | -27.16 | 53.255 | -82.53 | 8.3066 | 0.000 |
| UN | 0.099 | 0.021 | 4 | S355 | 35500 | , | 2.5000 | 0.4778 | 1.000 | 0.803 | 10635. | 0.0000 | 1292.8 | 1292.8 | 3879.7 | 3879.7 | 1103.5 | 0.009 |
| ok - | 7442 | 5 | F | CHS-CF 21 | 9.1X4 | 4 | 2.4918 | 2.4918 | 1.000 | 0.577 | -37.78 | 0.7110 | 0.7110 | -0.028 | -0.002 | 0.5706 | 0.0280 | - |
| OR | 0.054 | 0.002 | 1 | S355 | 35500 | | | 2.4918 | 1.000 | 0.960 | | 0.0000 | | | | | 58.516 | |
| ok - | 5563 | 6 | F | HEB28 | | 4 | 1.000.000.000 | 7.5000 | 1.000 | 0.000 | 0.0000 | Contraction of the local distance of the loc | -94.00 | 0.0000 | 0.0000 | | -> | -0.004 |
| on | 0.173 | 0.071 | 1 | S355 | 35500 | | 2.5000 | 7.5000 | 1.000 | 0.000 | 4650.5 | 0.0000 | 544.57 | 252.87 | 0.0000 | 834.79 | - | 0.030 |

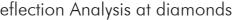
Reactions - ULS

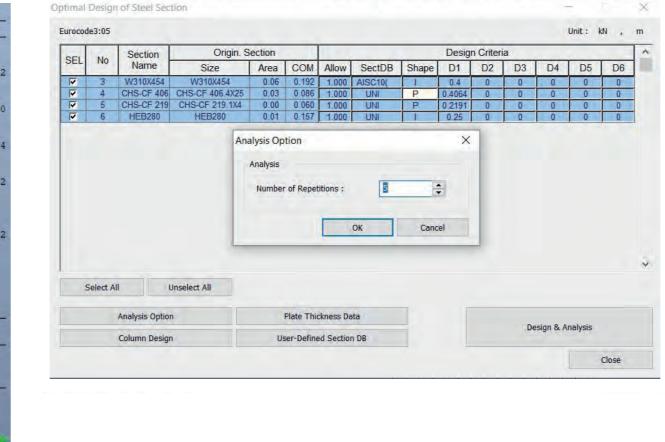
TOP PARTS ANALYSIS

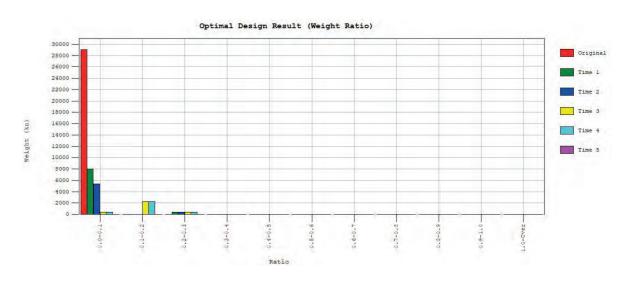






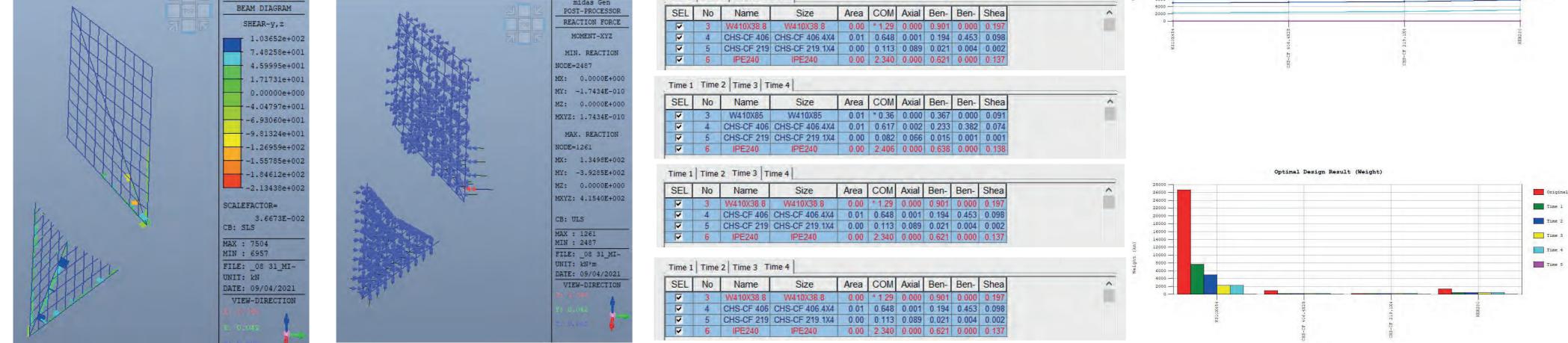


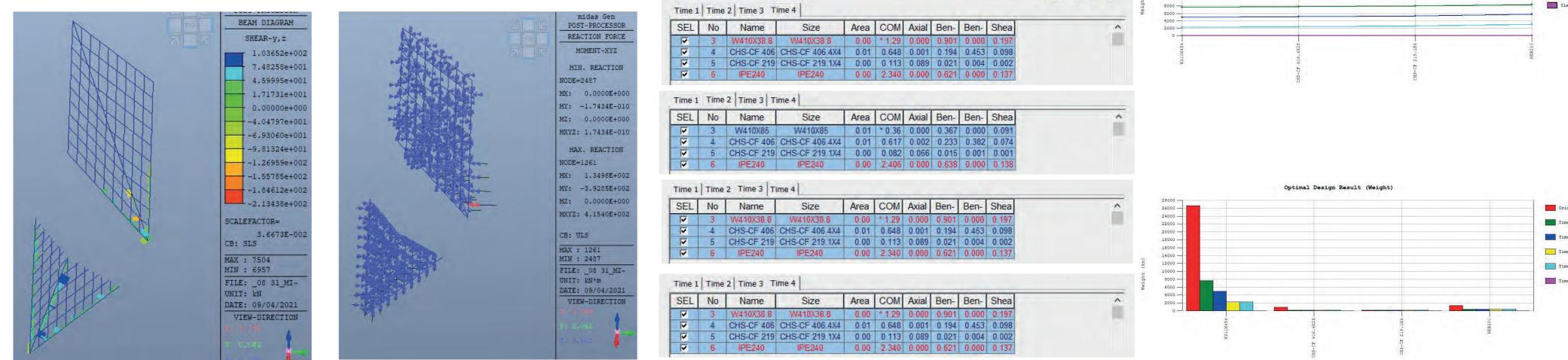




| Optimal Desi | gn Result (Weight S | um) | | |
|--------------|---------------------|-----|---|----------|
| | - | | | Original |
| | | | | Time 1 |
| | | | | Time 2 |
| | | | | Time 3 |
| | | | | Time 4 |
| | | | - | Time 5 |
| | | | | |









Shear Analysis at diamonds

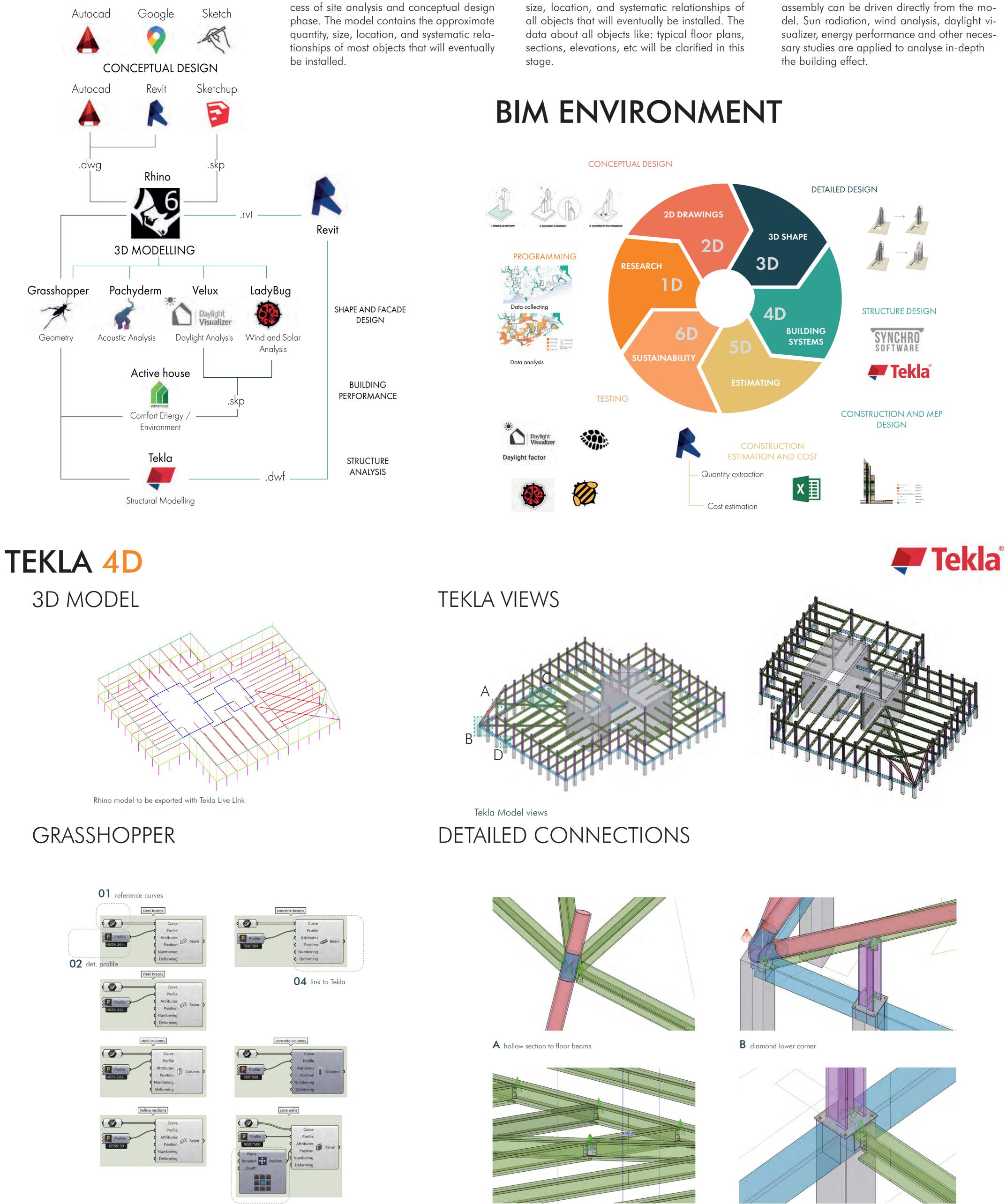
Reaction Analysis at diamonds

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|-----------------------------------|-------------------------------------|---|--|----------------------------------|--|---------|
| | | MARIA GRAZIA FOLLI CORRADO PECORA GIOVANNI DOTELLI FRANCESCO ROMANO | JUAN CARLOS MEDINA MARIA JOSE MONTERO | 10712731 | TORONTO AFFORDABLE | |



WORKFLOW

ANALYSIS



LEVEL OF DESIGN

100

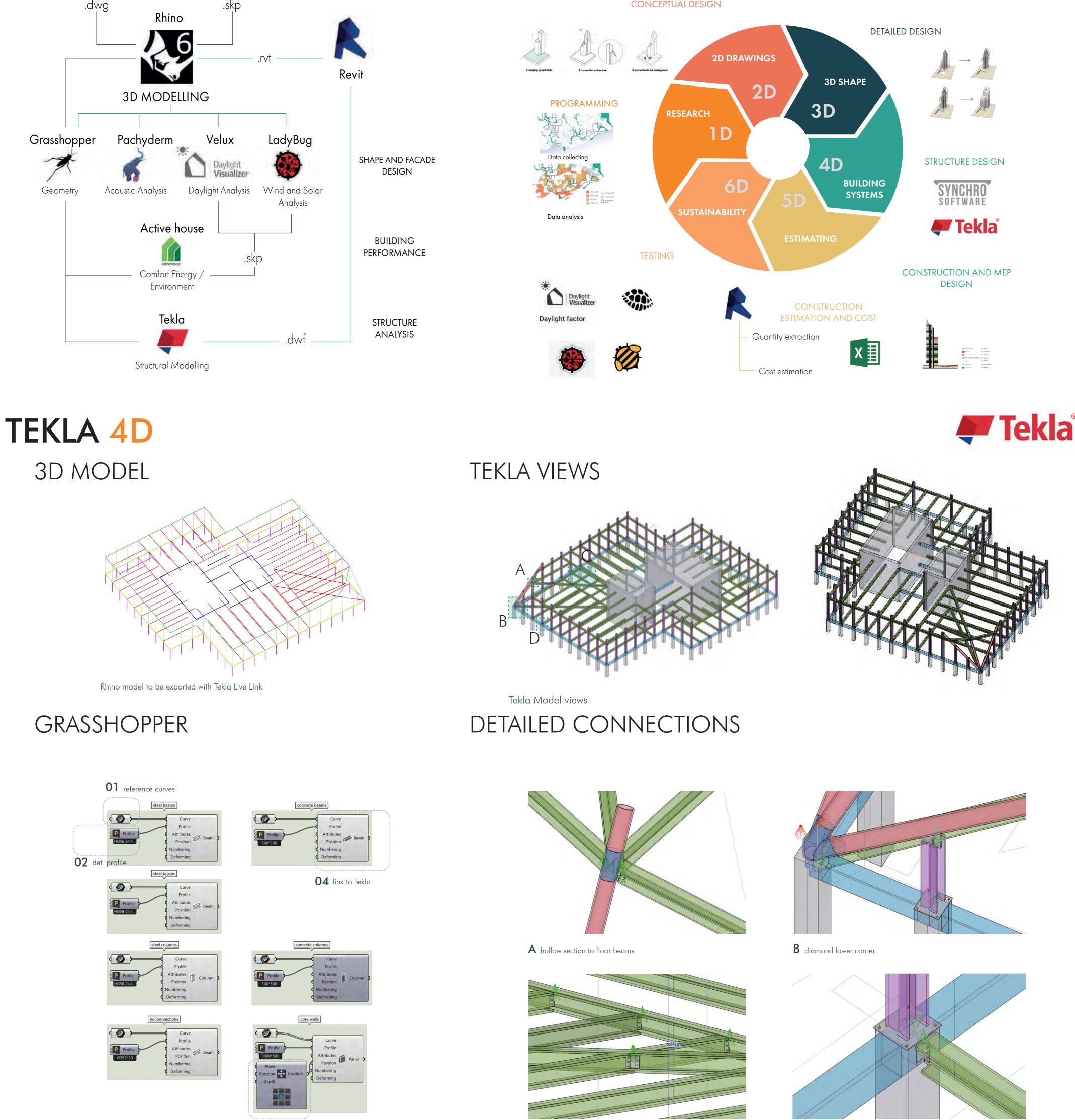
Building model ate this stage reflects the pro-

200

Building model contains the accurate quantity, size, location, and systematic relationships of

300

This stage is achieved when fabrication and





Tekla Live Llnk script

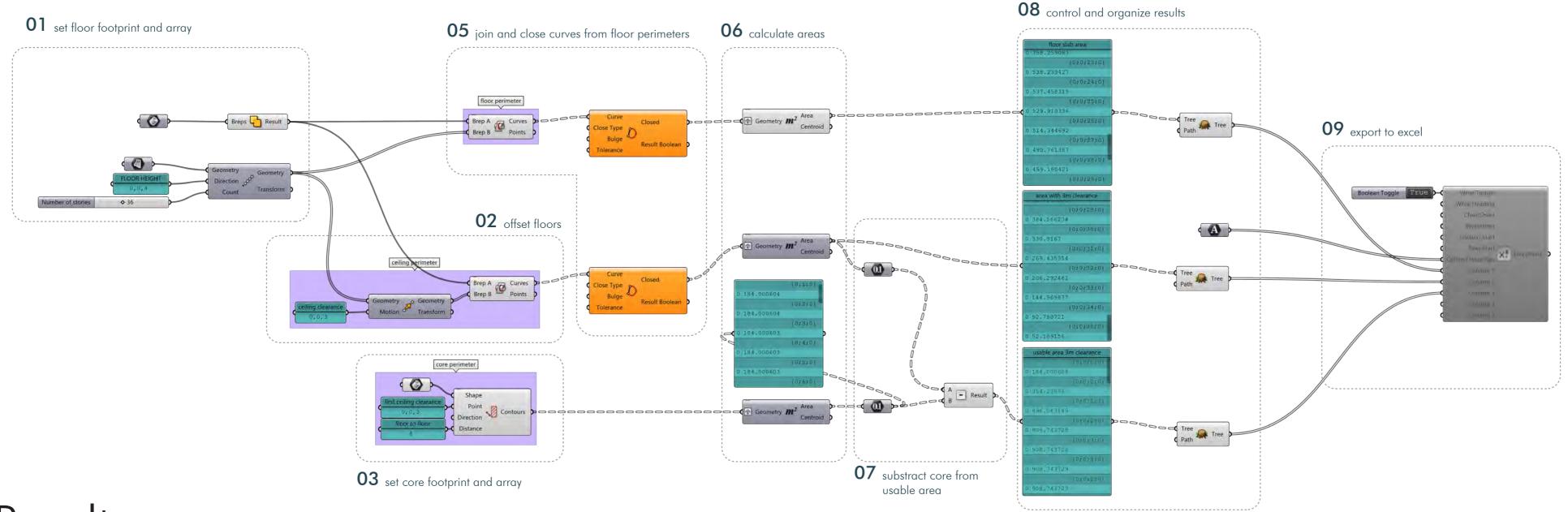
C typ. floor beam connection

D concrete to steel connection



GROUND FLOOR CONTROL AREA 5D

GRASSHOPPER



Results

| FLOOR NO. | SLAB AREA | AREA WITH CLEARANCE 3M | USABLE AREA (NO CORE) |
|--------------|-----------|---------------------------|--------------------------|
| | sqm | sqm | sqm |
| 1 | 1092.74 | 1092.74 | 908.74 |
| 2 | 1092.74 | 1092.74 | 908.74 |
| 3 | 1092.74 | 1092.74 | 908.74 |
| 4 | 1092.74 | 1092.74 | 908.74 |
| 5 | 1092.74 | 1092.74 | 908.74 |
| 6 | 1092.74 | 1092.74 | 908.74 |
| 7 | 1092.74 | 1092.74 | 908.74 |
| 8 | 1092.74 | 1092.74 | 908.74 |
| 9 | 1092.74 | 1092.74 | 908.74 |
| 10 | 1092.74 | 1092.74 | 908.74 |
| 11 | 1092.74 | 1092.74 | 908.74 |
| 12 | 1092.74 | 1092.74 | 908.74 |
| 13 | 1092.74 | 1092.74 | 908.74 |
| 14 | 1092.74 | 1092.74 | 908.74 |
| 15 | 1092.74 | 1087.78 | 903.78 |
| 16 | 1083.78 | 1064.78 | 880.78 |
| 17 | 1056.11 | 1023.07 | 839.07 |

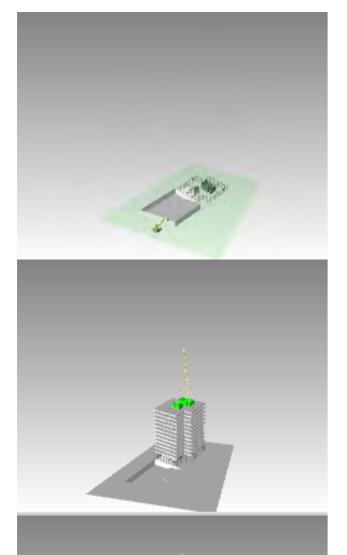
| FLOOR NO. | SLAB AREA | AREA WITH CLEARANCE 3M | USABLE AREA (NO CORE) |
|--------------|-----------|---------------------------|--------------------------|
| | sqm | sqm | sqm |
| 18 | 1009.72 | 962.65 | 818.35 |
| 19 | 944.62 | 883.51 | 739.21 |
| 20 | 860.80 | 785.65 | 641.35 |
| 21 | 758.26 | 538.24 | 393.94 |
| 22 | 538.24 | 538.09 | 393.79 |
| 23 | 537.46 | 532.55 | 388.25 |
| 24 | 529.91 | 518.99 | 406.53 |
| 25 | 514.34 | 497.41 | 384.95 |
| 26 | 490.76 | 467.81 | 428.41 |
| 27 | 459.16 | 430.20 | 416.89 |
| 28 | 419.54 | 384.57 | 371.26 |
| 29 | 371.91 | 330.92 | 317.61 |
| 30 | 316.25 | 269.44 | 256.13 |
| 31 | 253.52 | 206.29 | 192.98 |
| 32 | 190.72 | 144.97 | 131.66 |
| 33 | 130.84 | 92.78 | 79.47 |
| 34 | 81.55 | 52.19 | 38.88 |



| Results fro | om Excel |
|-------------|----------|
|-------------|----------|

SYNCHRO 6D BUILDING SIMULATION

3D Model



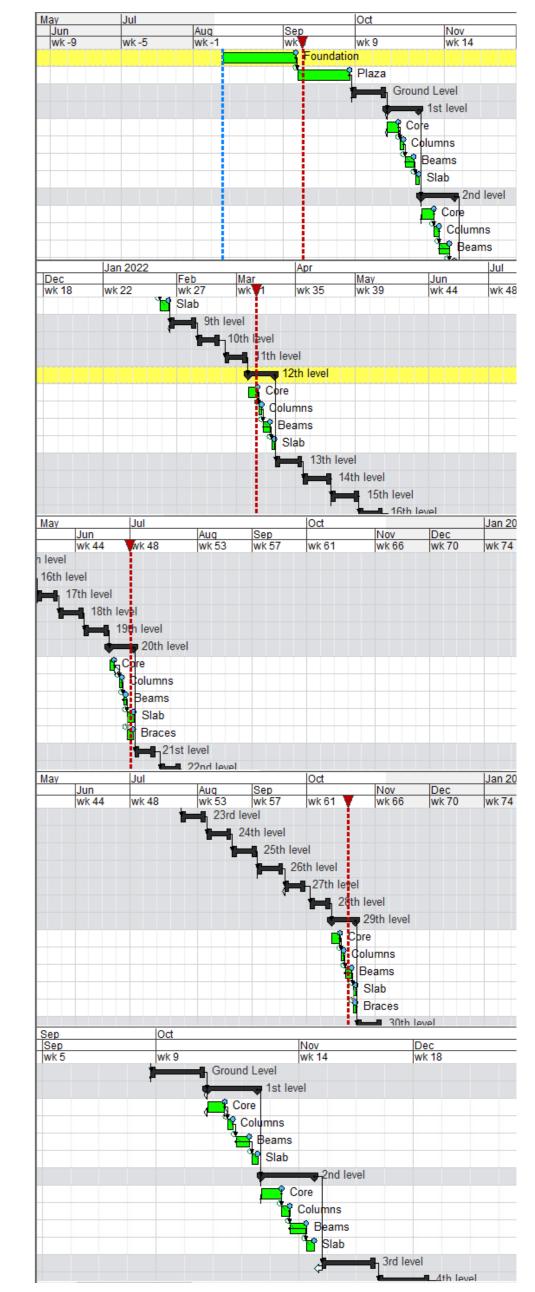
Task assignments

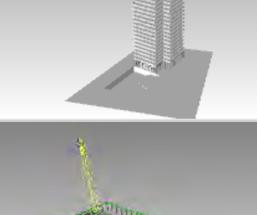
| ID | Name | Duration | Start | Finish | 3D Reso |
|--|---|----------------------------------|--|--|-------------------------------|
| ST00 | Foundation | 21d | 9:00 12/08/2021 | 17:00 09/09/2021 | 216 |
| ST00 | Plaza | 15d | 9:00 10/09/2021 (*) | 17:00 30/09/2021 (*) | 1 |
| ST00 | Ground Level | 9d | 14:56 01/10/2021 | 14:56 14/10/2021 | (135) |
| | ▲ 1st level | 9d | 9:00 15/10/2021 | 17:00 27/10/2021 | |
| ST00 | Core | 3d 3d | 9:00 15/10/2021 | 17:00 19/10/2021 | |
| | | | | | |
| ST00 | Columns | 2d | 9:00 20/10/2021 (*) | 17:00 21/10/2021 (*) | |
| ST00 | Beams | 2d | 9:00 22/10/2021 (*) | 17:00 25/10/2021 (*) | 73 |
| ST00 | Slab | 2d | 9:00 26/10/2021 (*) | 17:00 27/10/2021 (*) | 1 |
| | ✓ 2nd level | 9d | 14:56 28/10/2021 | 14:56 10/11/2021 | (139) |
| ST00 | Core | 3d | 14:56 28/10/2021 | 14:56 02/11/2021 | 11 |
| ST00 | Columns | 2d | 14:56 02/11/2021 (*) | 14:56 04/11/2021 (*) | 57 |
| ST00 | Beams | 2d | 14:56 04/11/2021 (*) | 14:56 08/11/2021 (*) | |
| 5100 | Beams | 20 | 14.50 04/11/2021 (*) | 14.50 08/11/2021 (*) | 70 |
| ID | Name | Duration | Start | Finish | 3D Reso. |
| ST00 | Slab | 2d | 16:41 28/01/2022 (*) | 16:41 01/02/2022 (*) | |
| | > 9th level | 9d | 9:00 02/02/2022 | 17:00 14/02/2022 | (139) |
| | 10th level | 9d | 9:00 15/02/2022 | 17:00 25/02/2022 | (130) |
| | It is a second secon | 9d | | 17:00 10/03/2022 | |
| | | | 9:00 28/02/2022 | | |
| | 12th level | 9d | 9:00 11/03/2022 | 17:00 23/03/2022 | |
| ST00 | Core | 3d | 9:00 11/03/2022 | 17:00 15/03/2022 | 11 |
| ST00 | Columns | 2d | 9:00 16/03/2022 (*) | 17:00 17/03/2022 (*) | 57 |
| ST00 | Beams | 2d | 9:00 18/03/2022 (*) | 17:00 21/03/2022 (*) | |
| этоо | Slab | 2d | 9:00 22/03/2022 (*) | 17:00 23/03/2022 (*) | |
| | ▷ 13th level | 9d | 9:00 24/03/2022 | 17:00 05/04/2022 | (130) |
| | | | | | |
| | > 14th level | 9d | 9:11 06/04/2022 | 9:11 19/04/2022 | |
| | 15th level | 9d | 14:47 19/04/2022 | 14:47 02/05/2022 | |
| | h 16th loval | hû | 16-40 02/05/2022 | 16-/0 13/05/2022 | |
| ID | Name | Duration | Start | Finish | 3D Reso |
| | ▷ 15th level | 9d | 14:47 19/04/2022 | 14:47 02/05/2022 | (194) |
| | ▷ 16th level | 9d | 16:40 02/05/2022 | 16:40 13/05/2022 | (129) |
| | 17th level | 9d | 9:00 16/05/2022 | | - |
| | , | | | 17:00 26/05/2022 | · · · |
| | 18th level | 9d | 9:00 27/05/2022 | 17:00 08/06/2022 | (126) |
| | 19th level | 9d | 9:00 09/06/2022 | 17:00 21/06/2022 | (128) |
| | ✓ 20th level | 9d | 9:00 22/06/2022 | 17:00 04/07/2022 | (118) |
| ST00 | Core | 3d | 9:00 22/06/2022 | 17:00 24/06/2022 | 11 |
| ST00 | Columns | 2d | 9:00 27/06/2022 (*) | 17:00 28/06/2022 (*) | 38 |
| ST00 | Beams | 2d | 9:00 29/06/2022 (*) | 17:00 30/06/2022 (*) | |
| | | | | | |
| ST00 | Slab | 2d | 9:00 01/07/2022 (*) | 17:00 04/07/2022 (*) | |
| ST00 | Braces | 1d, 2h, 21m | 11:13 01/07/2022 (*) | 13:34 04/07/2022 (*) | 22 |
| | 21st level | 9d | 9:00 05/07/2022 | 17:00 15/07/2022 | (49) |
| | > 22nd lovel | hD | 0.00 18/02/2022 | 17.00 28/07/2022 | (91) 3D |
| ID | Name | Duration | Start | Finish | Reso |
| | 23rd level | 9d | 9:00 29/07/2022 | 17:00 10/08/2022 | (82) |
| | 24th level | 9d | 9:00 11/08/2022 | 17:00 23/08/2022 | (84) |
| | 25th level | 9d | 9:00 24/08/2022 | 17:00 05/09/2022 | |
| | | | | | |
| | 26th level | 9d | 9:21 06/09/2022 | 9:21 19/09/2022 | · · |
| | 27th level | 9d | 9:00 20/09/2022 | 17:00 30/09/2022 | (78) |
| | 28th level | 9d | 9:00 03/10/2022 | 17:00 13/10/2022 | (59) |
| | ✓ 29th level | 9d | 9:00 14/10/2022 | 17:00 26/10/2022 | (70) |
| ST01 | Core | 3d | 9:00 14/10/2022 | 17:00 18/10/2022 | 10 |
| ST01 | Columns | 2d | 9:00 19/10/2022 (*) | 17:00 20/10/2022 (*) | |
| | | | | | |
| ST01 | Beams | 2d | 9:00 21/10/2022 (*) | 17:00 24/10/2022 (*) | |
| ST01 | Slab | 2d | 9:00 25/10/2022 (*) | 17:00 26/10/2022 (*) | |
| ST01 | Braces | 1d, 2h, 21m | 11:13 25/10/2022 (*) | 13:34 26/10/2022 (*) | |
| | > 30th loval | hû | 0.00 27/10/2022 | 17.00 08/11/2022 | |
| ID | Name | Duration | Start | Finish | 3D Reso |
| | ▷ Ground Level | 9d | 14:56 01/10/2021 | 14:56 14/10/2021 | (135) |
| ST00 | ✓ 1st level | 9d | 9:00 15/10/2021 | 17:00 27/10/2021 | |
| ST00 | | 3d 3d | 9:00 15/10/2021 | 17:00 19/10/2021 | - |
| | Core | JU | | | |
| ST00 | Core | 64 | 9:00 20/10/2021 (*) | 17:00 21/10/2021 (*) | |
| ST00 ST00 | Columns | 2d | | | 72 |
| ST00 | | 2d 2d | 9:00 22/10/2021 (*) | 17:00 25/10/2021 (*) | |
| ST00 ST00 | Columns | | | 17:00 25/10/2021 (*) 17:00 27/10/2021 (*) | |
| ST00 ST00 ST00 | Columns Beams | 2d | 9:00 22/10/2021 (*) | | 1 |
| ST00 ST00 ST00 ST00 | Columns Beams Slab A 2nd level | 2d 2d 9d | 9:00 22/10/2021 (*) 9:00 26/10/2021 (*) 14:56 28/10/2021 | 17:00 27/10/2021 (*) 14:56 10/11/2021 | 1 (139) |
| ST00 ST00 ST00 ST00 | Columns Beams Slab 2nd level Core | 2d 2d 9d 3d | 9:00 22/10/2021 (*) 9:00 26/10/2021 (*) 14:56 28/10/2021 14:56 28/10/2021 | 17:00 27/10/2021 (*) 14:56 10/11/2021 14:56 02/11/2021 | 1 (139) 11 |
| ST00 ST00 ST00 ST00 ST00 | Columns Beams Slab 2nd level Core Columns | 2d 2d 9d 3d 2d | 9:00 22/10/2021 (*) 9:00 26/10/2021 (*) 14:56 28/10/2021 14:56 28/10/2021 14:56 02/11/2021 (*) | 17:00 27/10/2021 (*) 14:56 10/11/2021 14:56 02/11/2021 14:56 04/11/2021 (*) | 1 (139) 11 57 |
| ST00 ST00 ST00 ST00 ST00 ST00 ST00 | Columns Beams Slab 2nd level Core Columns Beams | 2d 2d 9d 3d 2d 2d | 9:00 22/10/2021 (*) 9:00 26/10/2021 (*) 14:56 28/10/2021 14:56 28/10/2021 14:56 02/11/2021 (*) 14:56 04/11/2021 (*) | 17:00 27/10/2021 (*) 14:56 10/11/2021 14:56 02/11/2021 14:56 04/11/2021 (*) 14:56 08/11/2021 (*) | 1 (139) 11 57 70 |
| ST00 ST00 ST00 | Columns Beams Slab 2nd level Core Columns | 2d 2d 9d 3d 2d | 9:00 22/10/2021 (*) 9:00 26/10/2021 (*) 14:56 28/10/2021 14:56 28/10/2021 14:56 02/11/2021 (*) | 17:00 27/10/2021 (*) 14:56 10/11/2021 14:56 02/11/2021 14:56 04/11/2021 (*) | 1 (139) 11 57 70 |

Link to video here:

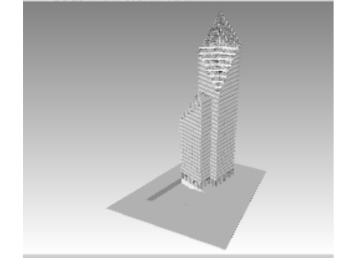


Schedule





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| CARCA CONSIGNATION DATA | |



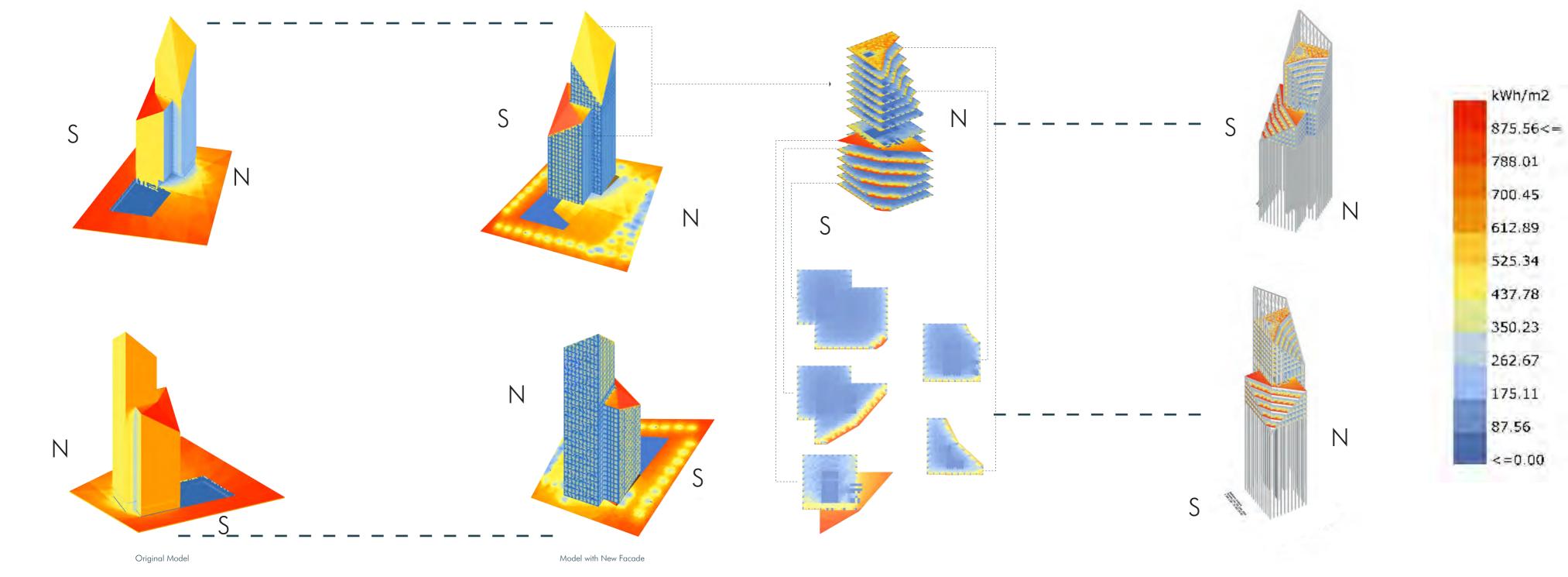




LADYBUG 6D

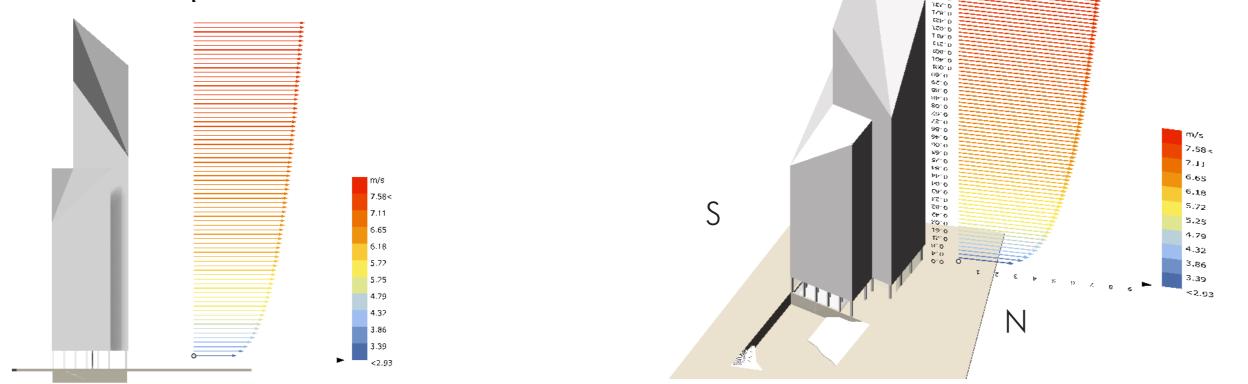


RADIATION ANALYSIS



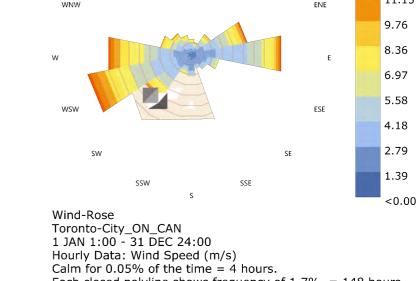
WIND ANALYSIS

East facade





m/s 13.94< 12.55 11.15



Each closed polyline shows frequency of 1.7%. = 148 hours.

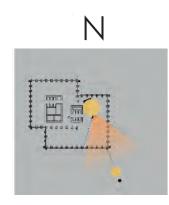
VELUX DAYLIGHT VISUALIZER 6D

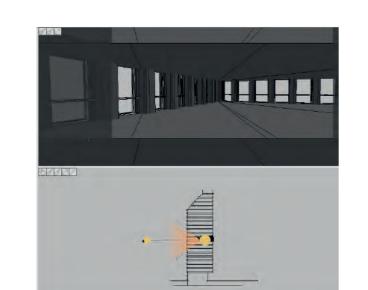
VIZ

ILLUMINANCE ANALYSIS

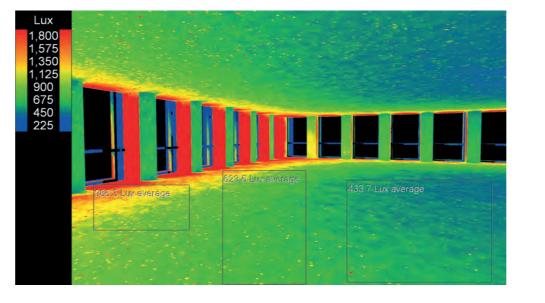
Daylight Visualizer Daylight factor

Level +22.00

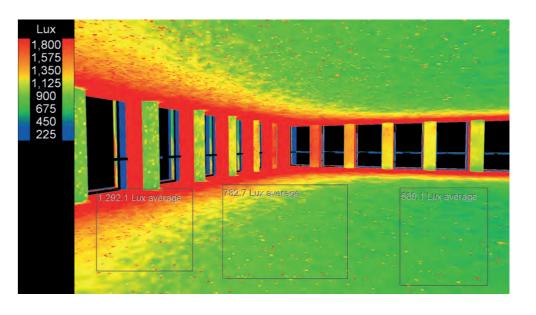


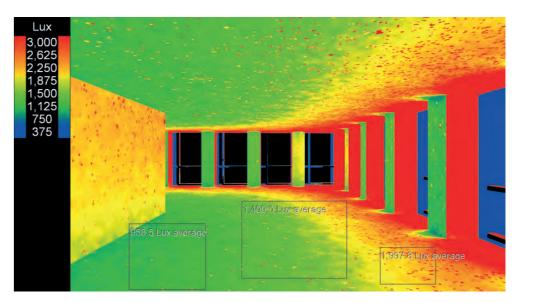


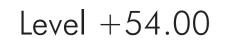


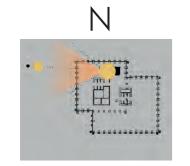


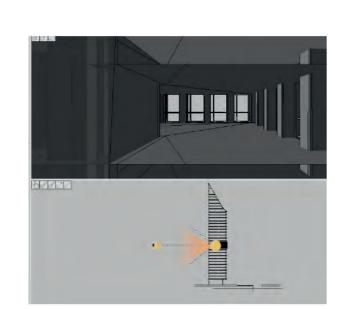
Julyl at 12.00

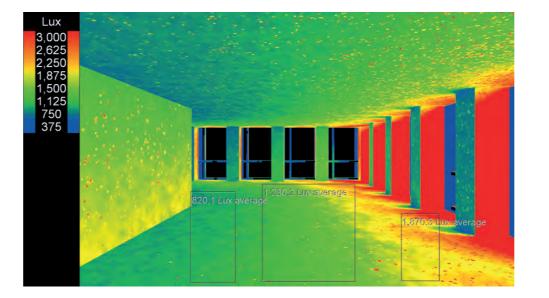








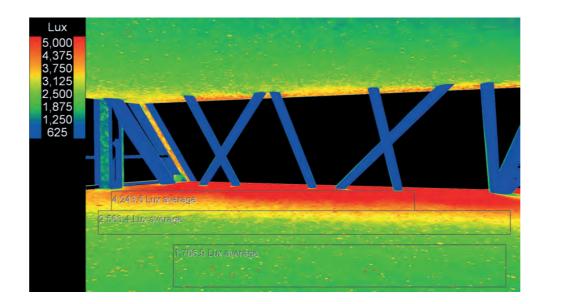


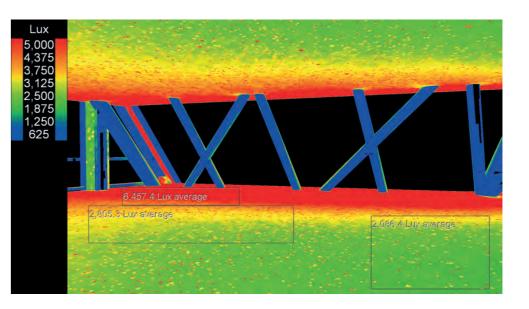


Level +122.00







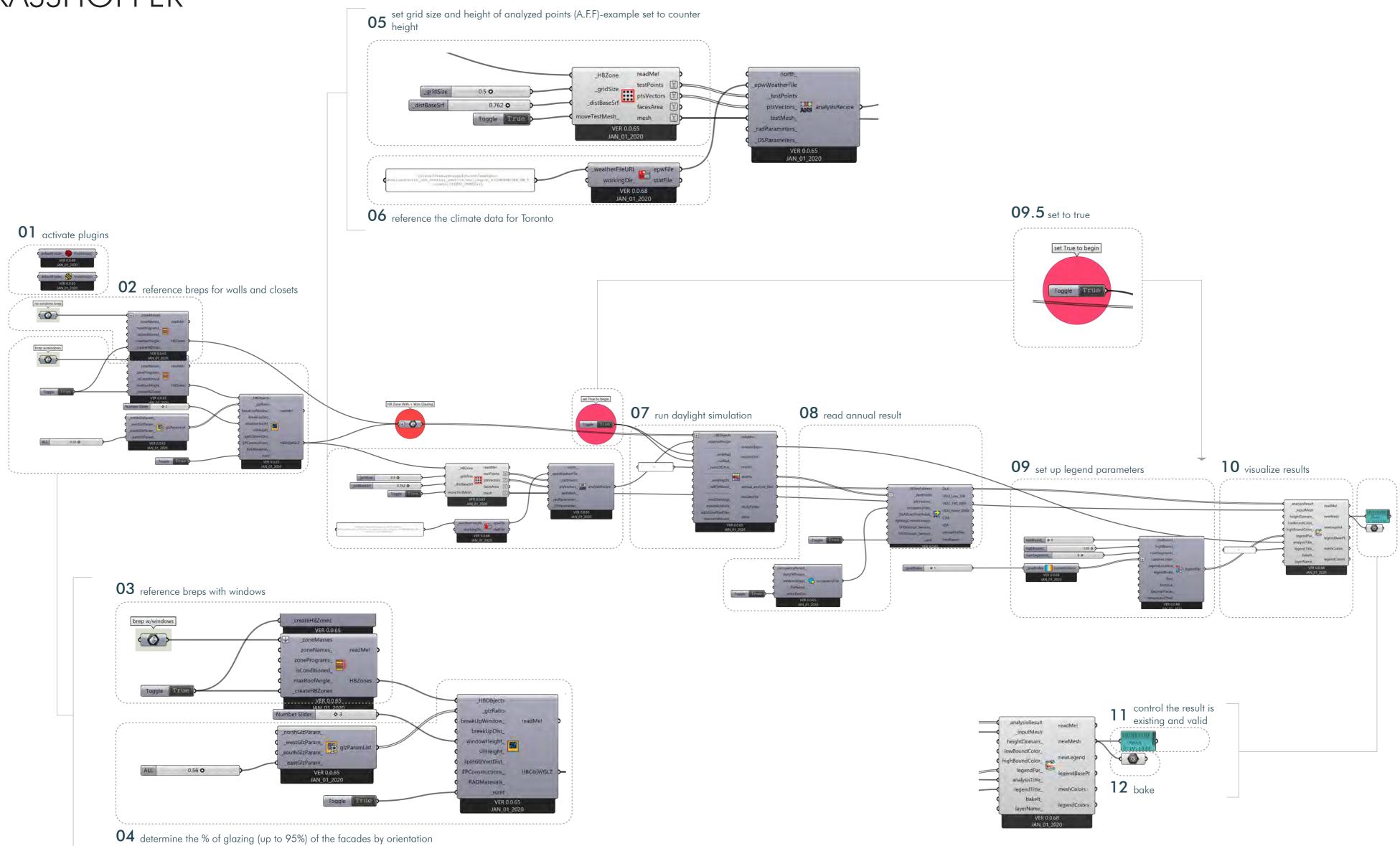




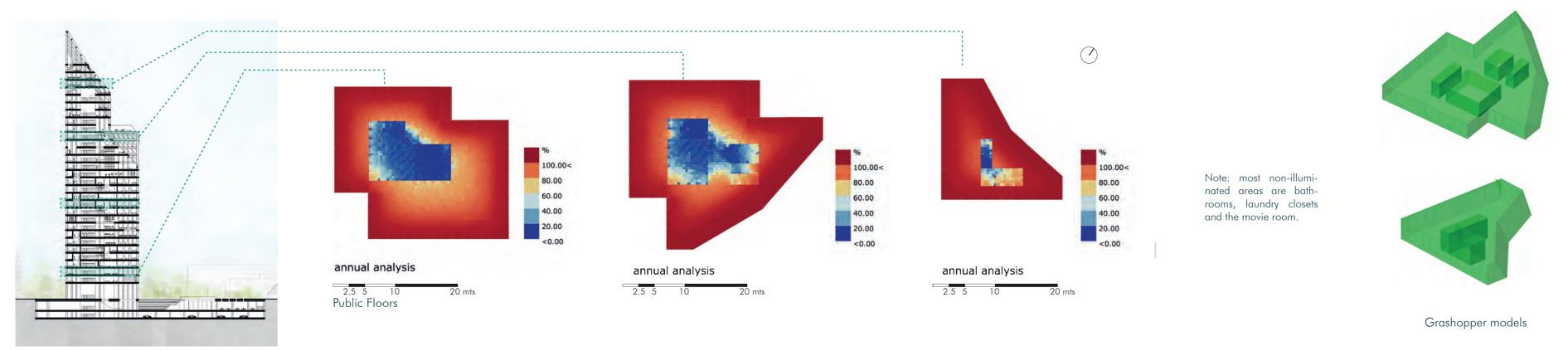
HONEYBEE 6D ANNUAL DAYLIGHT EXPOSURE



GRASSHOPPER

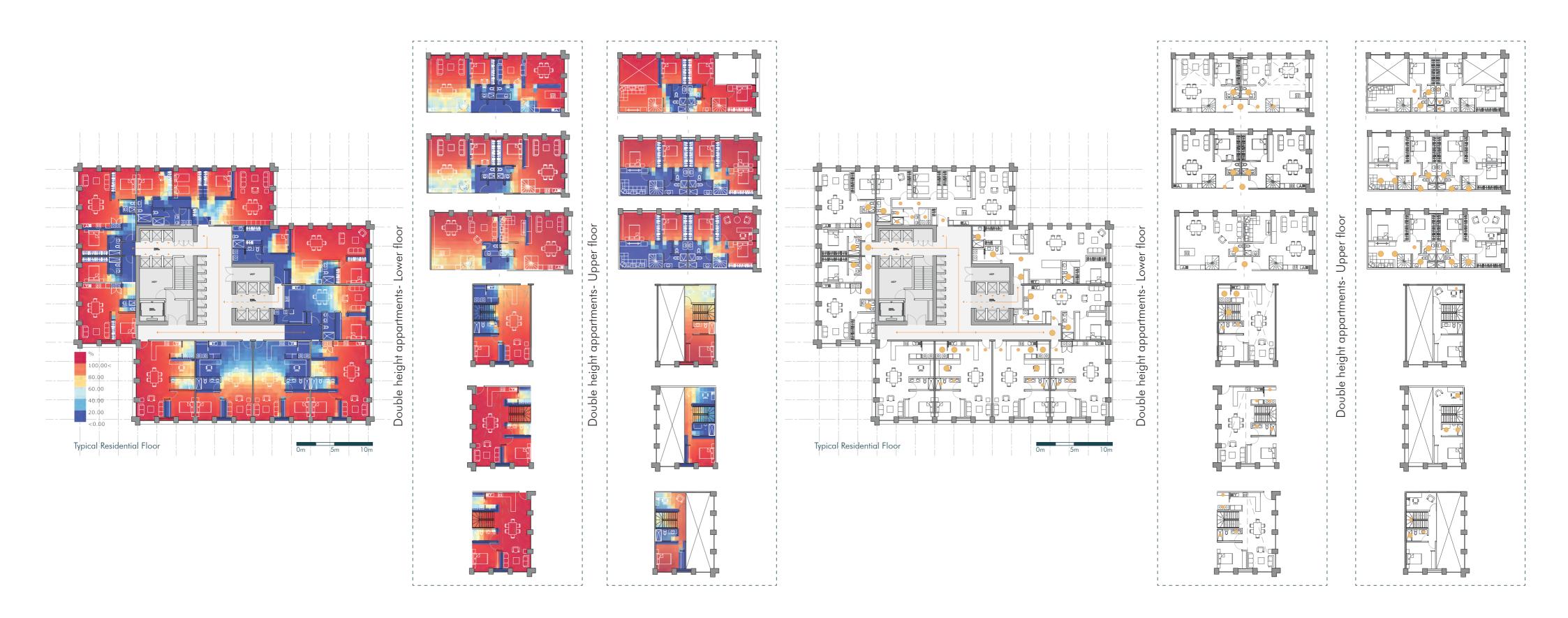


ANNUAL ANALYSIS BY FLOOR



TYPICAL FLOOR PLAN RESULTS

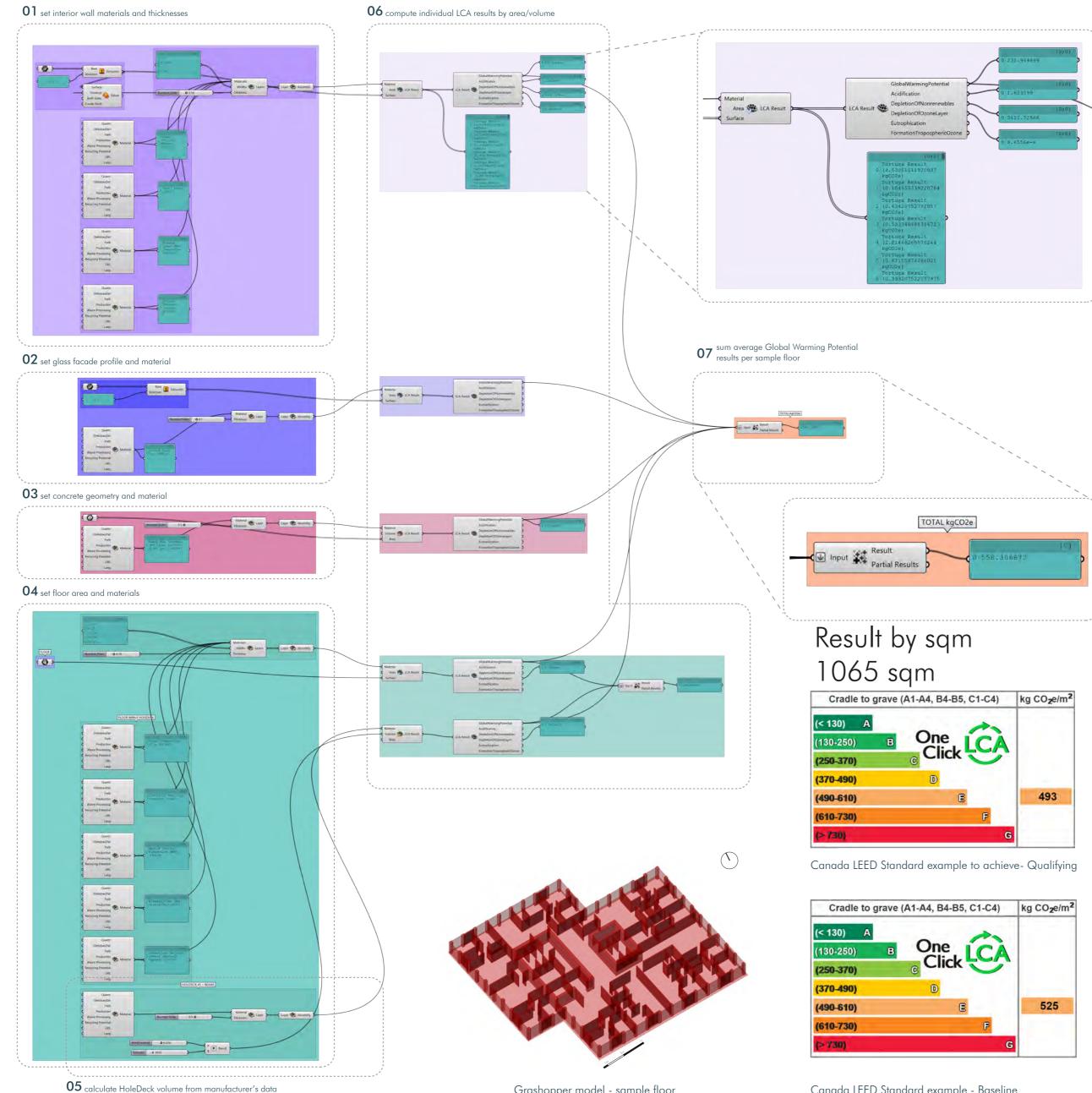
OPPORTUNITY AREAS





TORTUGA 6D LCA (LIFE CYCLE ASSESMENT)

GRASSHOPPER



Option 1

| | Global | | Depletion of | Depletion o |
|---|----------------------|---------------|--------------------|----------------|
| BETTER OPTION | Warming Potential | Acidification | Non- renewables | Ozone Layer |
| | kgCO2 | kgSO2 | MJ | kgFCF11 |
| INTERIOR WALLS Drywall / Natural Gypsum Steel Studs Mineral Fiber Batt Insulation Drywall / Natural Gypsum | 231.99 | 1.62 | 3412.7 | 8.60E-06 |
| FAÇADE Triple pane IGU | 89.51 | 0.4 | 1254 | 9.37E-07 |
| COLUMNS AND CORE Ready Mix Concrete (BF Slag) | 10.99 | 0.046 | 11.33 | 1.54E-08 |
| FLOOR/CEILING Vinyl Composition Tile Sub-Floor Smoothing Compound Fiber Glass Board Insulation Mineral Fiber Batt Insulation Acoustical Ceiling Panels (Natural Gypsum) | 284.33 | 2.05 | 4483.74 | 9.86E-06 |
| Holedeck 45 with Beams: Ready Mix Concrete (BF Slag) | 20.81 | 0.088 | 210.7 | 2.92E-08 |
| TOTAL | 637.63 | 4.204 | 9372.47 | 1.944E-0 |

Option 2 (best result)

| | Global | | Depletion of | Depletion of |
|--|-----------|---------------|------------------|--------------|
| BEST OPTION | Warming | Acidification | Non- | Ozone |
| | Potential | | renewables MJ | Layer |
| INTERIOR WALLS | kgCO2 | kgSO2 | IVIJ | kgFCF11 |
| INTERIOR WALLS Drywall / Natural Gypsum Steel Studs Mineral Fiber Batt Insulation Drywall / Natural Gypsum | 231.99 | 1.62 | 3412.7 | 8.60E-06 |
| FAÇADE | 89.51 | 0.4 | 1254 | 9.37E-07 |
| Triple pane IGU | | | | |
| COLUMNS AND CORE Ready Mix Concrete (BF Slag) | 10.99 | 0.046 | 11.33 | 1.54E-08 |
| | | | | |
| FLOOR/CEILING Vinyl Composition Tile Sub-Floor Smoothing Compound Medium Density Fiberboard (MDF) Mineral Fiber Batt Insulation Acoustical Ceiling Panels (Natural Gypsum) | 204.98 | 1.77 | 4118.78 | 4.48E-06 |
| | | | | |
| Holedeck 45 with Beams: Ready Mix Concrete (BF Slag) | 20.81 | 0.088 | 210.7 | 2.92E-08 |
| | | | | |

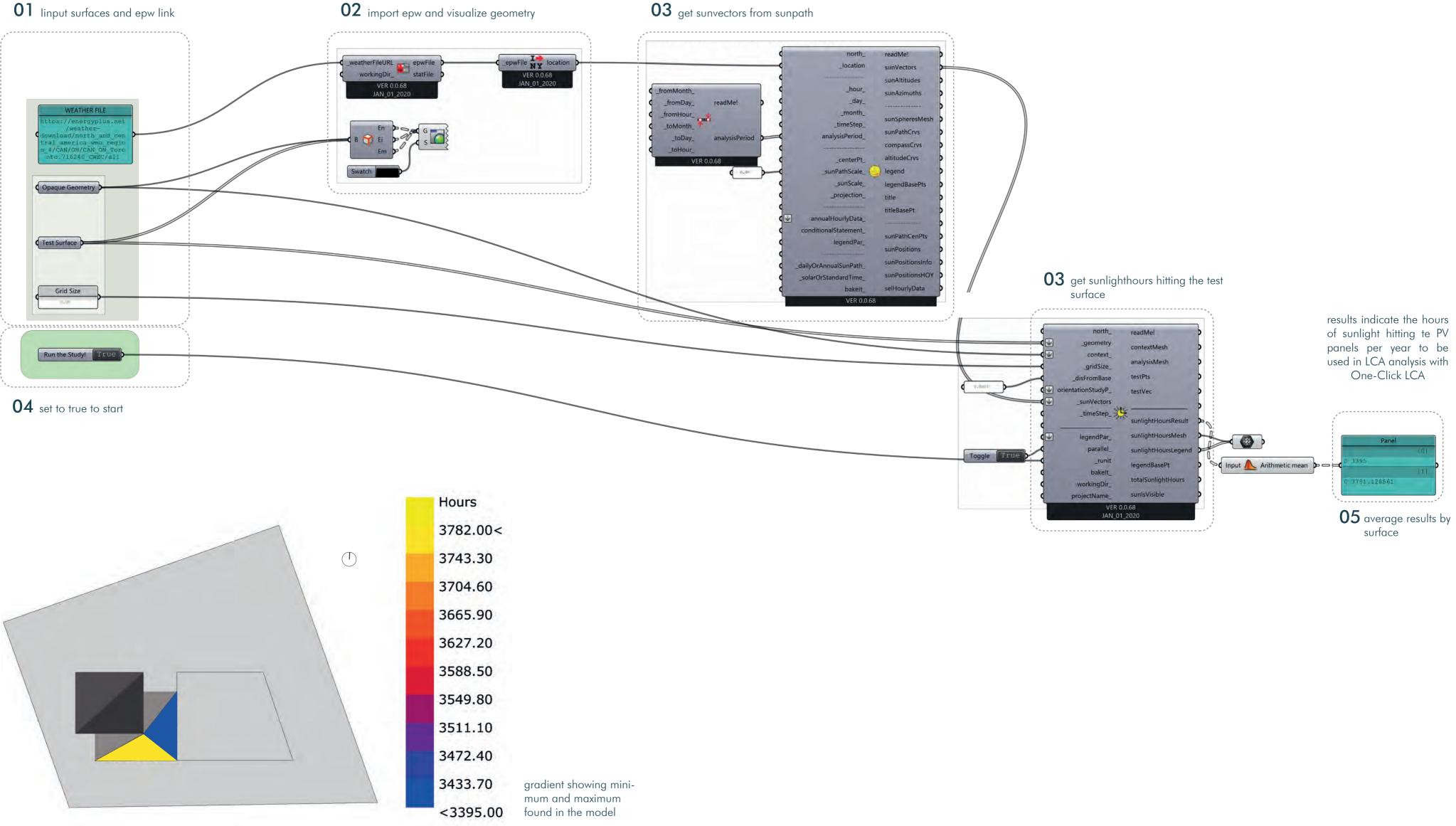
| Cradle to g | rave (A1-A4, B4-B5, C1-C4) | kg CO ₂ e/m ² |
|-------------|----------------------------|-------------------------------------|
| (< 130) A | | |
| (130-250) | One LCA | |
| (250-370) | | |
| (370-490) | D | |

Grashopper model - sample floor

Canada LEED Standard example - Baseline

PV PANELS POTENTIAL ANALYSIS 6D

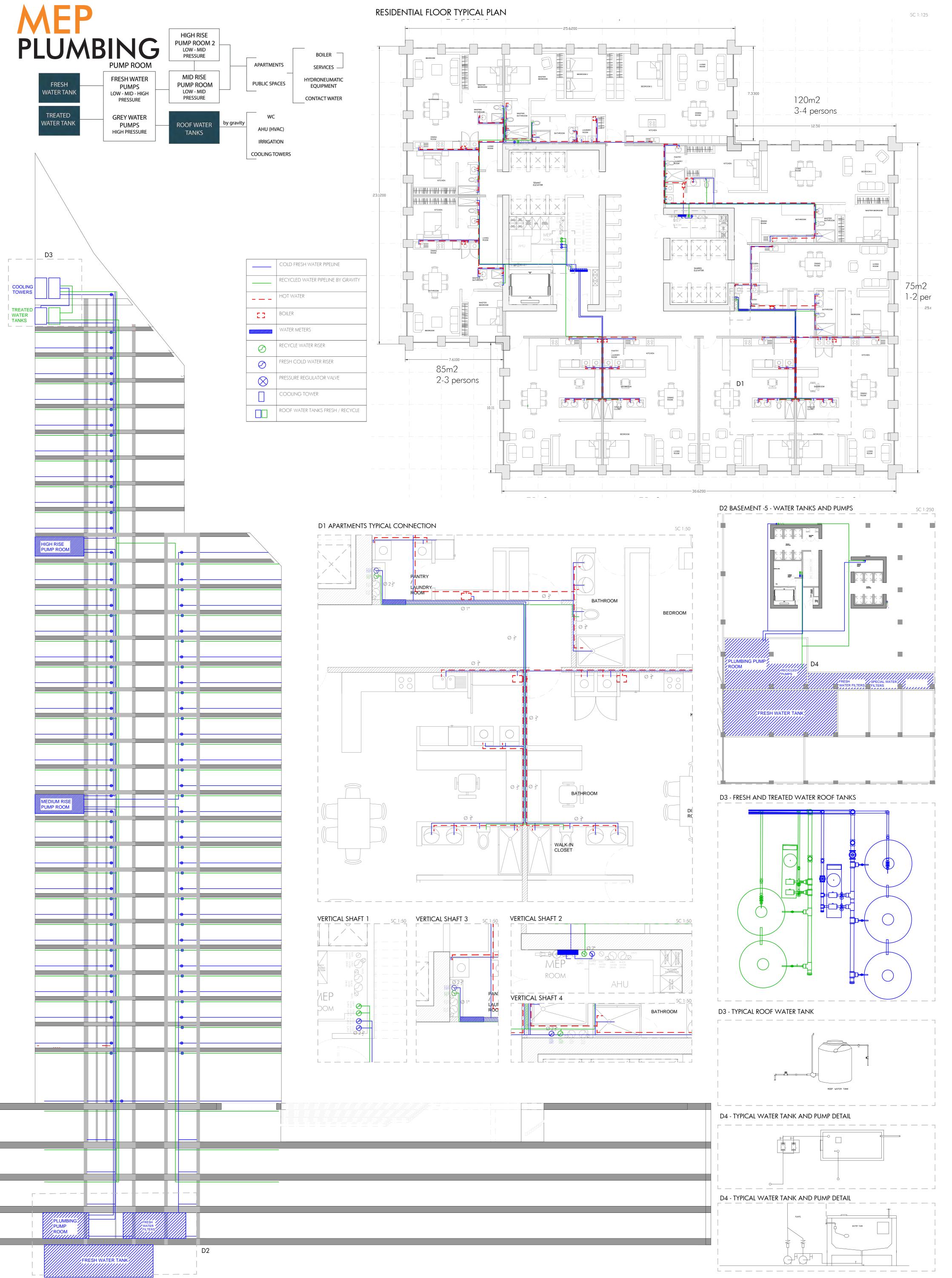


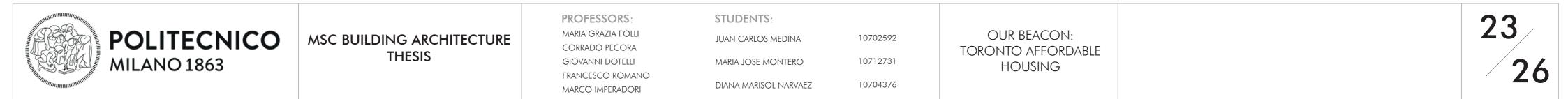


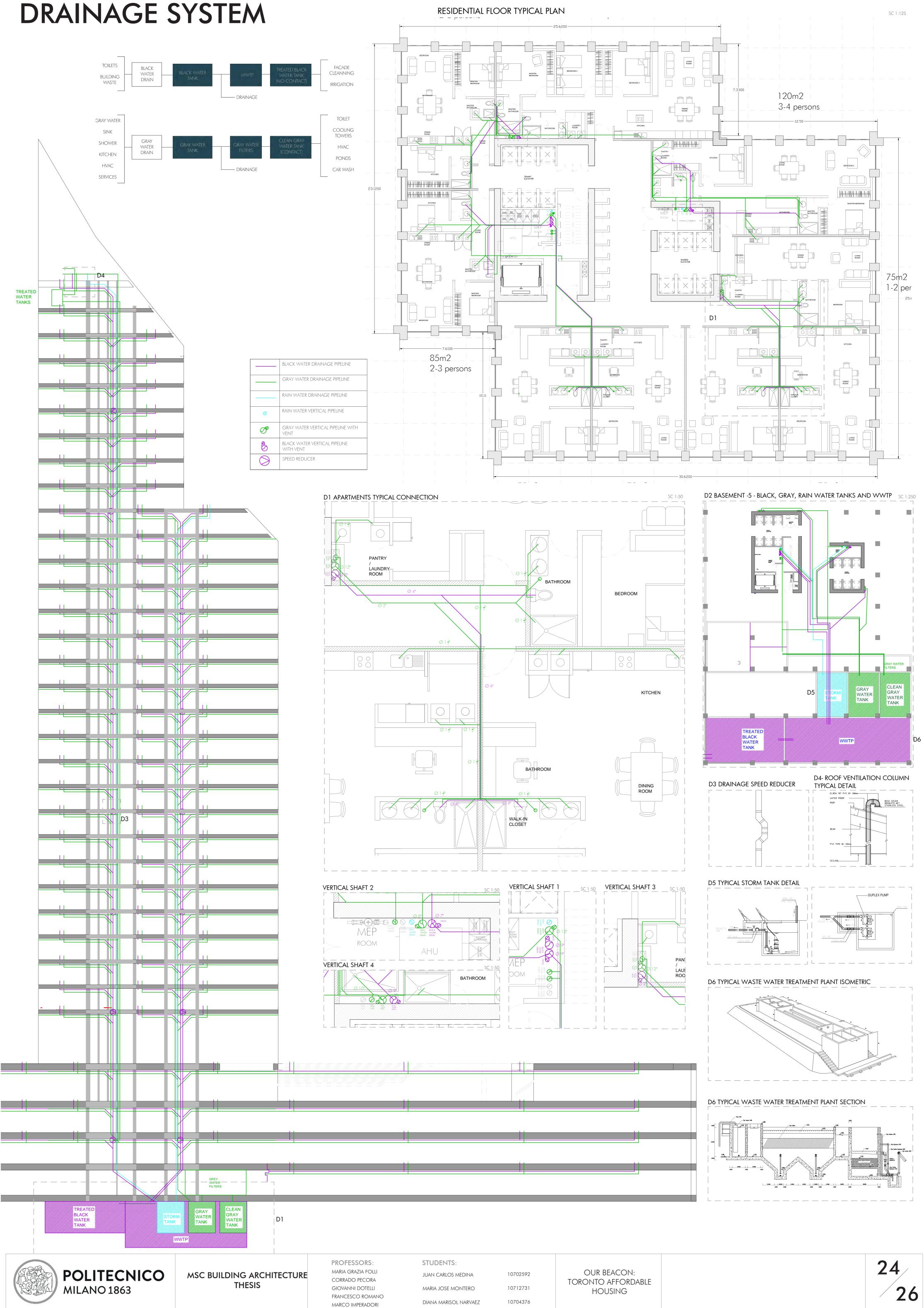
results indicate the hours of sunlight hitting te PV panels per year to be used in LCA analysis with One-Click LCA

SunlightHours Analysis

| POLITECNICO MILANO 1863 MSC BUILDING ARCHITECTURE THESIS | PROFESSORS: MARIA GRAZIA FOLLI CORRADO PECORA GIOVANNI DOTELLI FRANCESCO ROMANO MARCO IMPERADORI | STUDENTS: JUAN CARLOS MEDINA MARIA JOSE MONTERO DIANA MARISOL NARVAEZ | 10702592 10712731 10704376 | OUR BEACON: TORONTO AFFORDABLE HOUSING | | 22 26 |
|--|---|---|----------------------------------|--|--|----------|
|--|---|---|----------------------------------|--|--|----------|

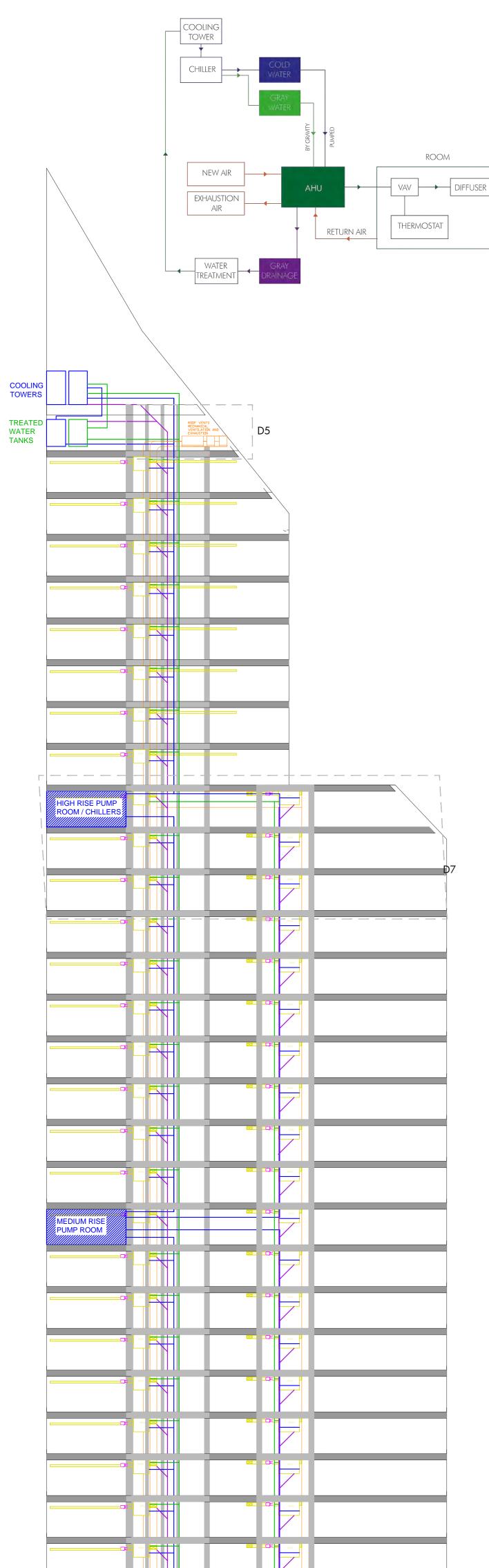


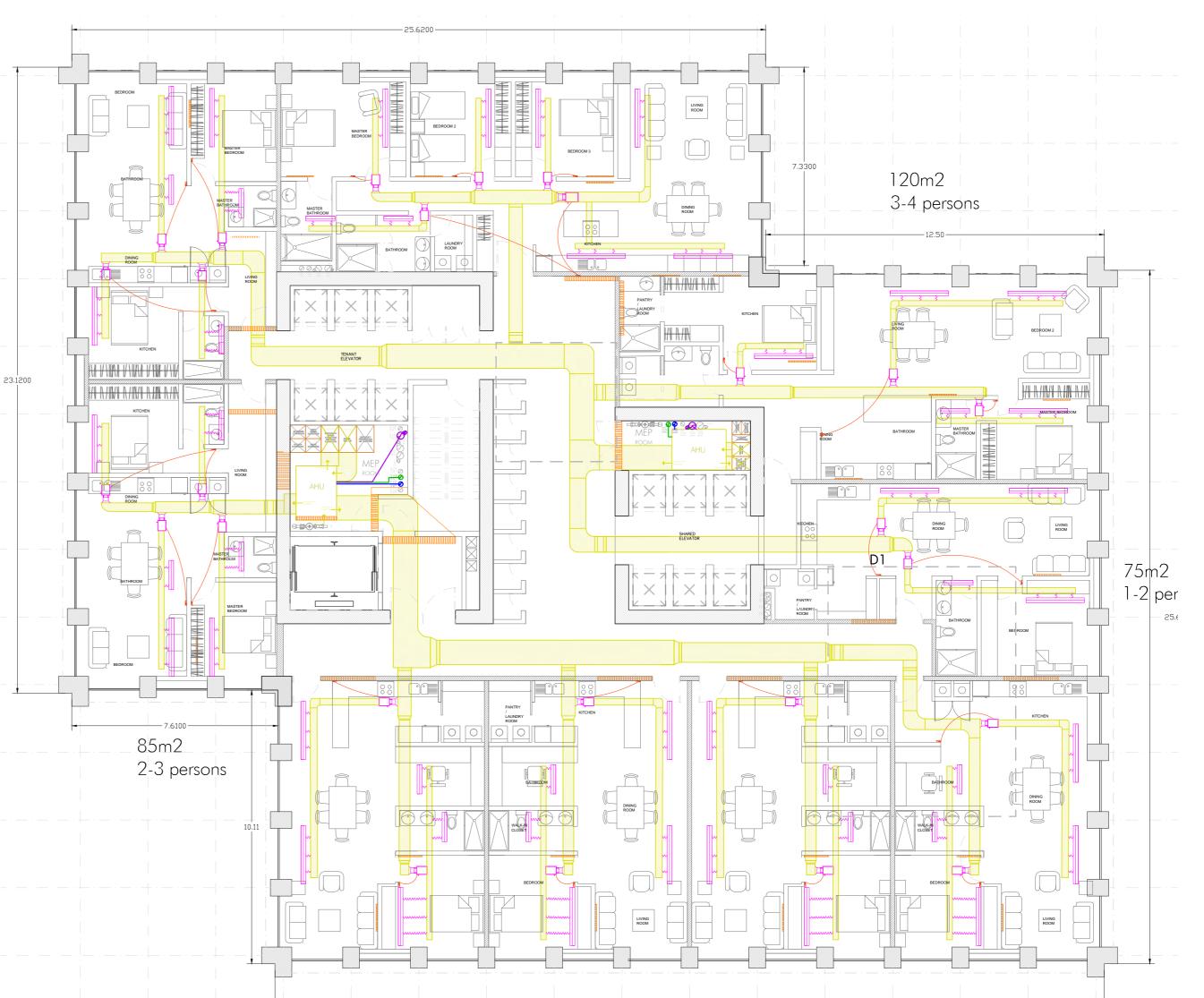


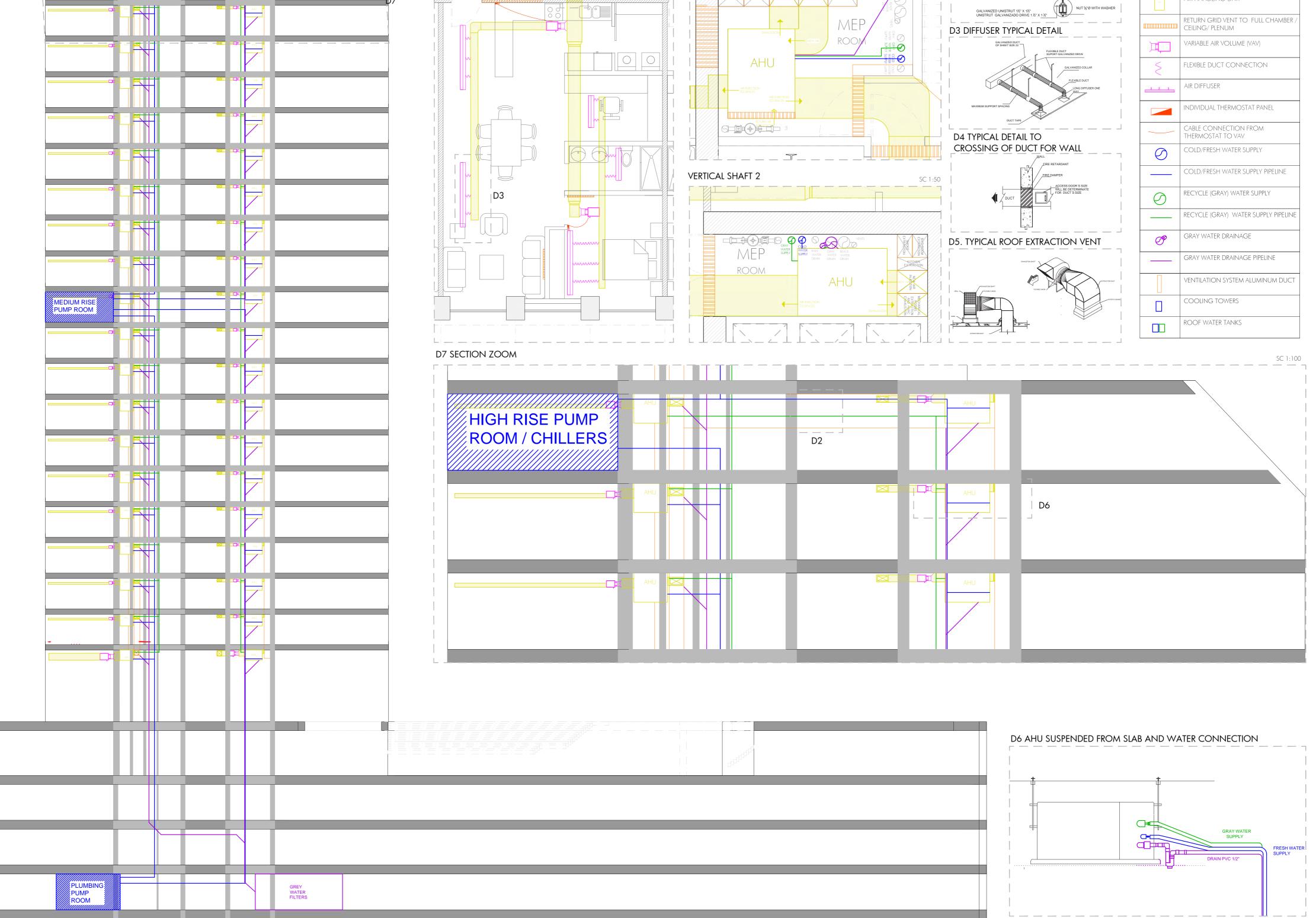


HVAC SYSTEM

RESIDENTIAL TYPICAL FLOOR PLAN







D1 APARTMENTS TYPICAL CONNECTION

30.6200

Ø

SC 1:50 VERTICAL SHAFT 3

VERTICAL SHAFT 1

BATHROC XTRACTI

KITCHEN XTRASTION SMOKE

SC 1:100

D4

D2 TYPICAL SUPPORT DETAIL FOR

DUCT LINER INSULATION 1"

ALUMINUM DUCT HVAC SUPPLIER

AIR DUCT SHAFT VERTICAL

AIR HANDLING UNIT

RECTANGULAR DUCTS



ELECTRICAL SYSTEM

LIGHTNING

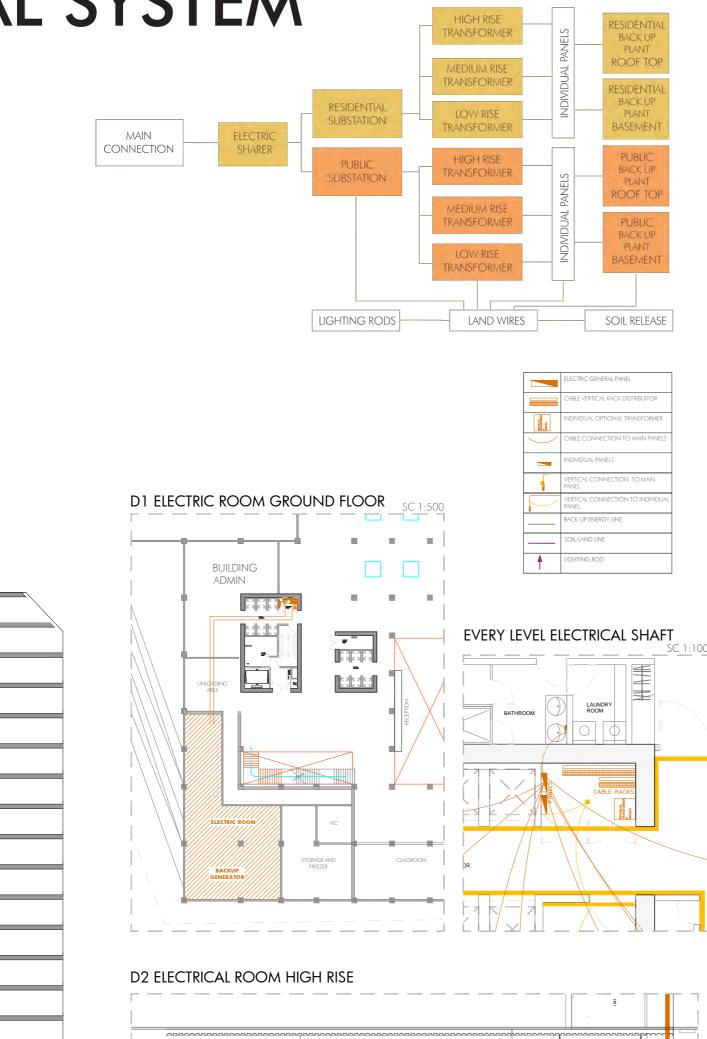
ECTRIC ROOM

- A

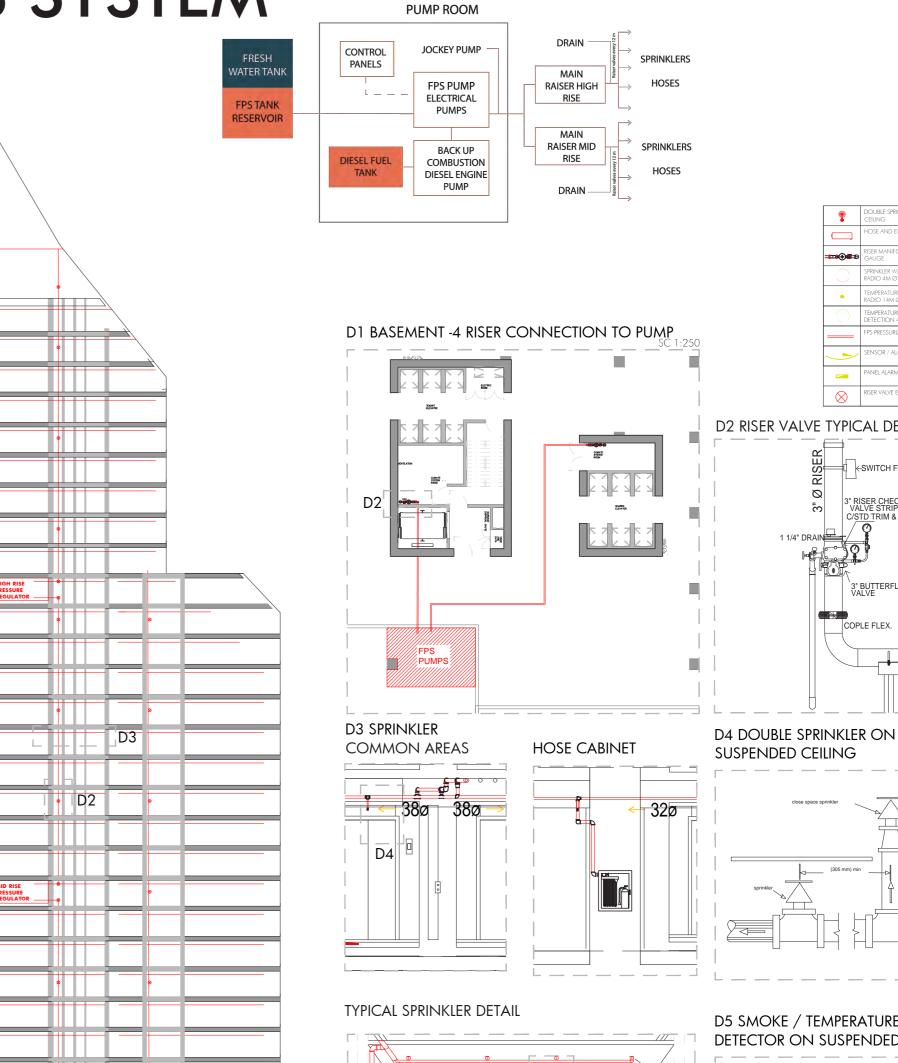
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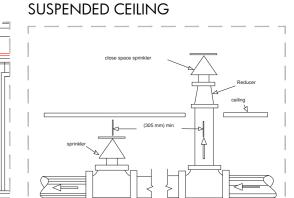
D2

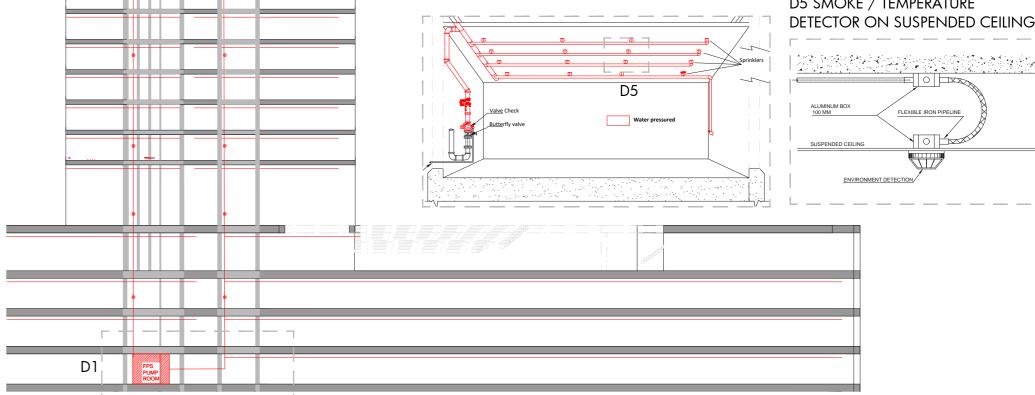


FPS SYSTEM

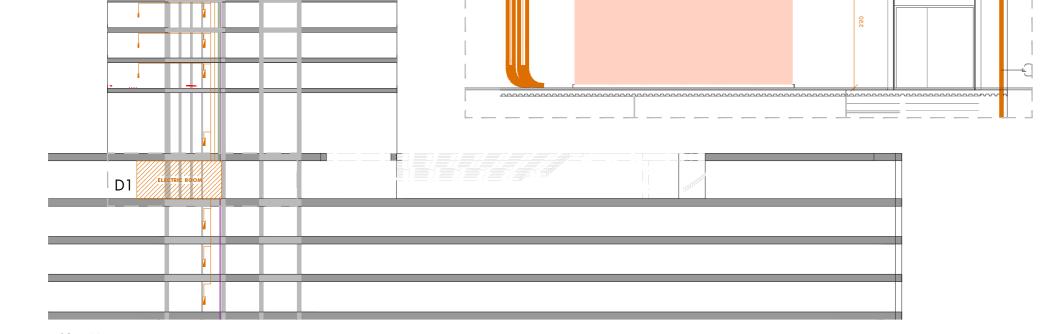


| Γ | P | DOUBLE SPRINKLER ON SUSPENDED |
|---|---------------------|---|
| - | • | CEILING HOSE AND EXTINGUISHER CABINET |
| - | ₩ ⊕ ∰⊐₽ | RISER MANIFORLD VALVE AND PRESSURE GAUGE |
| - | C | SPRINKLER WATER DEFLECTOR RADIO 4M Ø |
| - | • | TEMPERATURE / SMOKE DETECTOR RADIO 14M Ø |
| - | \bigcirc | TEMPERATURE / SMOKE RADIO DETECTION 4M Ø |
| - | | FPS PRESSURIZE WATER LINE 3*Ø |
| | | SENSOR / ALARM CABLE CONNECTION |
| - | _ | PANEL ALARM SYSTEM |
| - | \otimes | RISER VALVE EVERY 12 M |
| | = | |
| | 3" RI | SWITCH FLOW SER CHECK UL/FM 2 LVE STRIP TO TRIM & GAUGES |
| | 3" RI VA C/S' | SWITCH FLOW |
| | | SWITCH FLOW |
| | | SWITCH FLOW SER CHECK UL/FM 2 IVE STRIP TD TRIM & GAUGES |



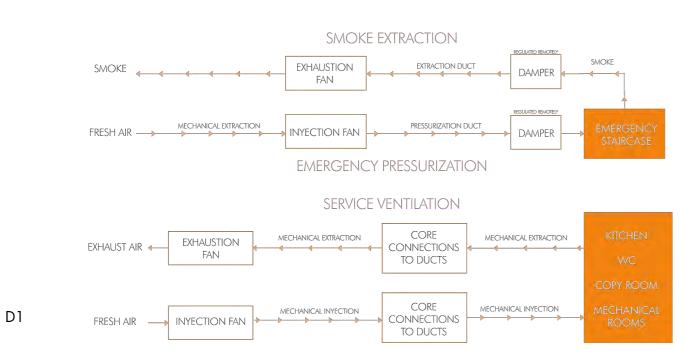


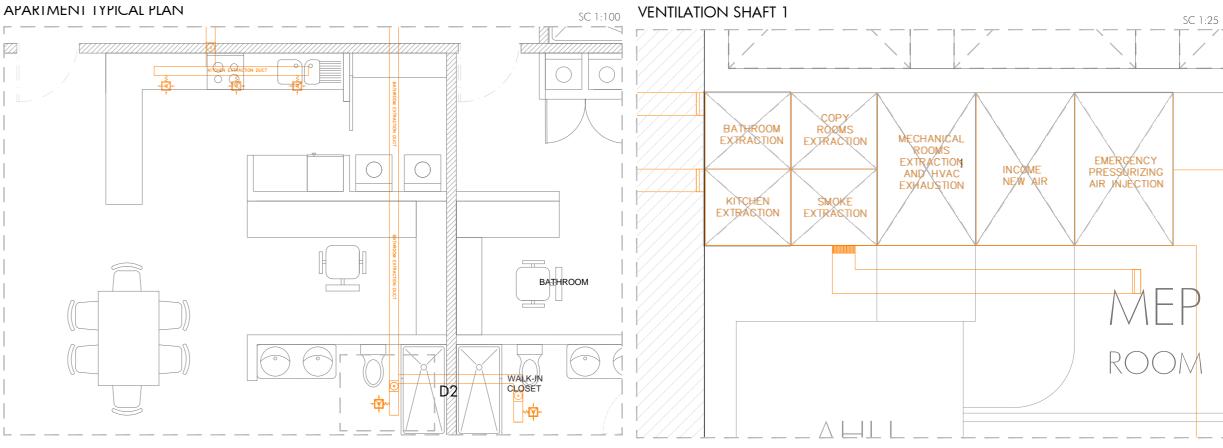
D5 SMOKE / TEMPERATURE DETECTOR ON SUSPENDED CEILING



SC 1:500

VENTILATION SYSTEM

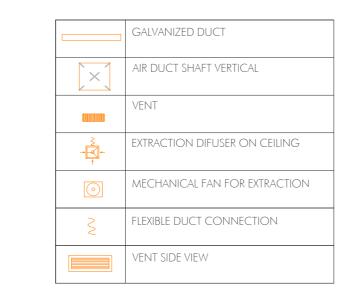


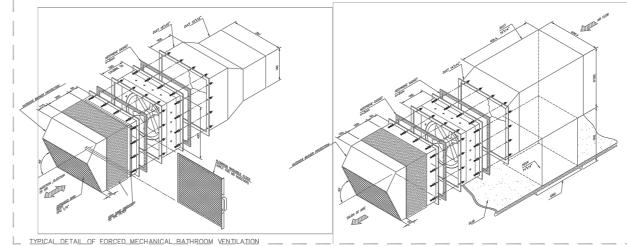


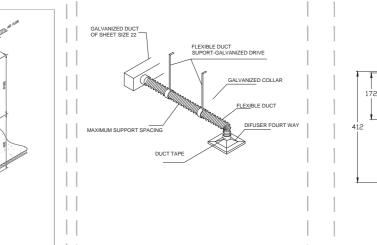
D1 TYPICAL DETAL OF EXHAUSTION FANS ON ROOF

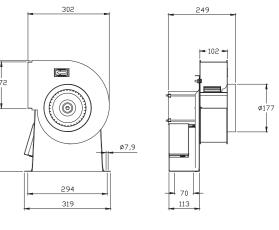
D2 DETAIL INSTALATION FLEXIBLE DUCT TO DIFUSER

D1 EXHAUSTION MOTOR

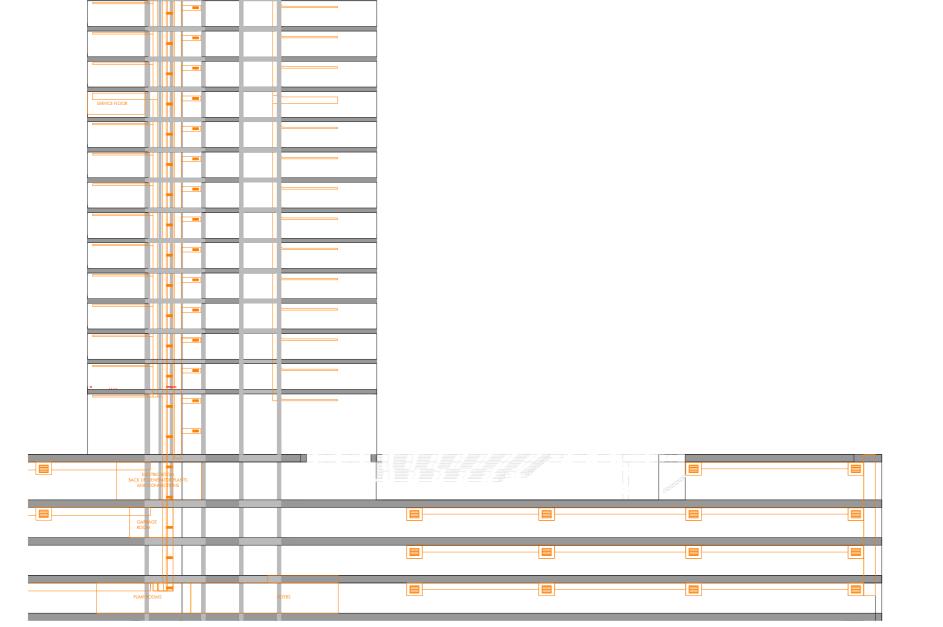


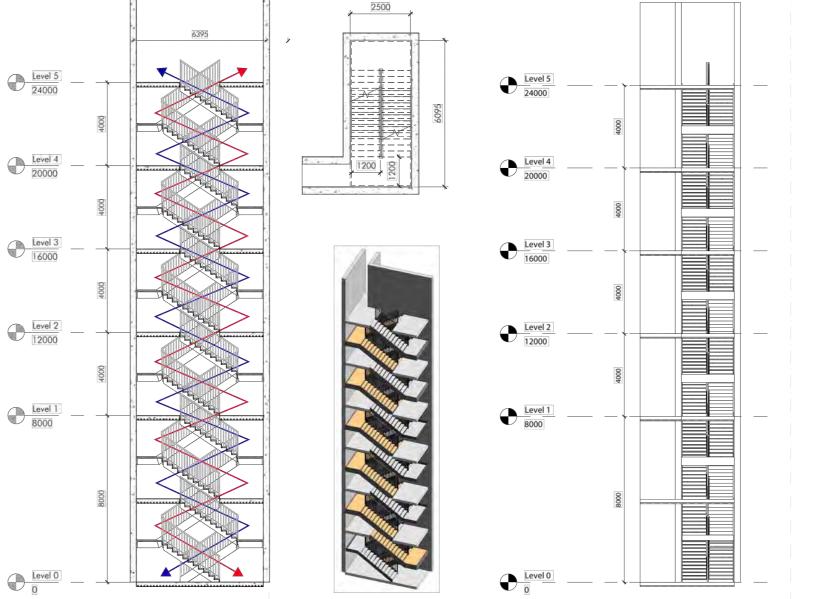






EMERGENCY STAIRCASE





SC 1:500

| | POLITECNICO MILANO 1863 | |
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| MSC BUILDING ARCHITECTURE | |
|---------------------------|--|
| THESIS | |

| PROFESSORS: | STUDENTS: | |
|--------------------|-----------------------|--|
| MARIA GRAZIA FOLLI | JUAN CARLOS MEDINA | |
| CORRADO PECORA | | |
| GIOVANNI DOTELLI | MARIA JOSE MONTERO | |
| FRANCESCO ROMANO | | |
| MARCO IMPERADORI | DIANA MARISOL NARVAEZ | |

OUR BEACON: TORONTO AFFORDABLE HOUSING

10702592

10712731

10704376

26 26